

EPFL

GaN

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Physics of Materials -4g

screw + mixed

Chapter 10: TEM techniques for characterizing dislocations

Masters Course PHYS-307

Fall 2025

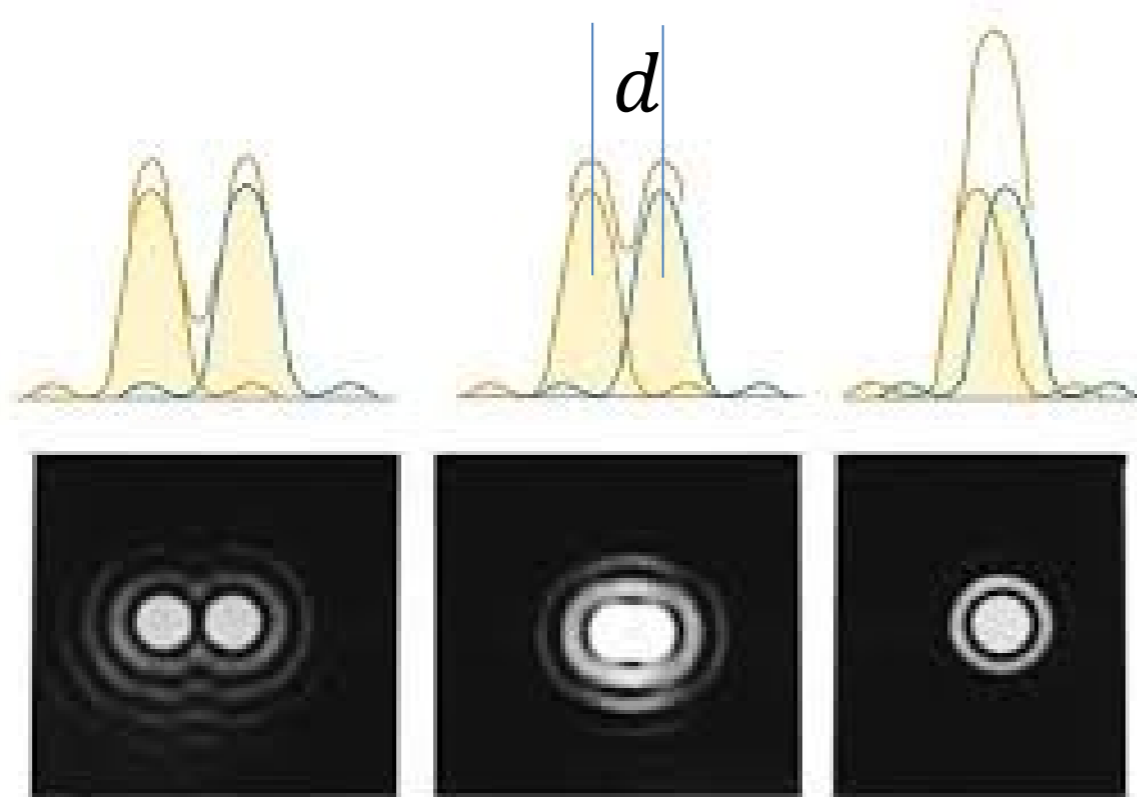
Electron Wavelengths in Electron Microscopes

<i>Electron charge (e)</i>	-1.602 x 10 ⁻¹⁹ C	non relativistic (<50keV)
<i>1 eV</i>	1.602 x 10 ⁻¹⁹ J	$\lambda = \frac{h}{(2m_0eV)^{1/2}}$
<i>Electron rest mass (m₀)</i>	9.109 x 10 ⁻³¹ kg	Relativistic correction
<i>Electron rest energy (m₀c²)</i>	511 keV	
<i>Kinetic energy (charge x tension)</i>	1.602 x 10 ⁻¹⁹ Nm (per 1 volt)	$\lambda = \frac{h}{\left[2m_0eV\left(1 + \frac{eV}{2m_0c^2}\right)\right]^{1/2}}$
<i>Plank's constant (h)</i>	6.626 x 10 ⁻³⁴ N-m-s	
<i>1 Ampere</i>	1 C/sec	
<i>Light speed in vacuum (c)</i>	2.998 x 10 ⁸ m/sec	

Accelerating voltage [KV]	Nonrelativistic λ [nm]	Relativistic λ [nm]	Mass [x m₀]	Velocity [x 10⁸ m/s]
1	0.03879	0.03878	1.002	0.13
10	0.01227	0.01221	1.02	0.42
80	0.00434	0.00418	1.157	1.1
200	0.00274	0.00251	1.391	1.59
300	0.00224	0.00197	1.587	1.82
1000	0.00123	0.00087	2.957	2.44

Diffraction Limited Resolution

Raleigh's Criterion



Airy Diffraction Disks

Green light : $\lambda \approx 532$ nm,

β (objective collection angle) ~ 1 rad

$n = 1.7$ for oil immersion lens

*** $d = 200$ nm

Electrons 200 keV : $\lambda \approx 0.00251$ nm

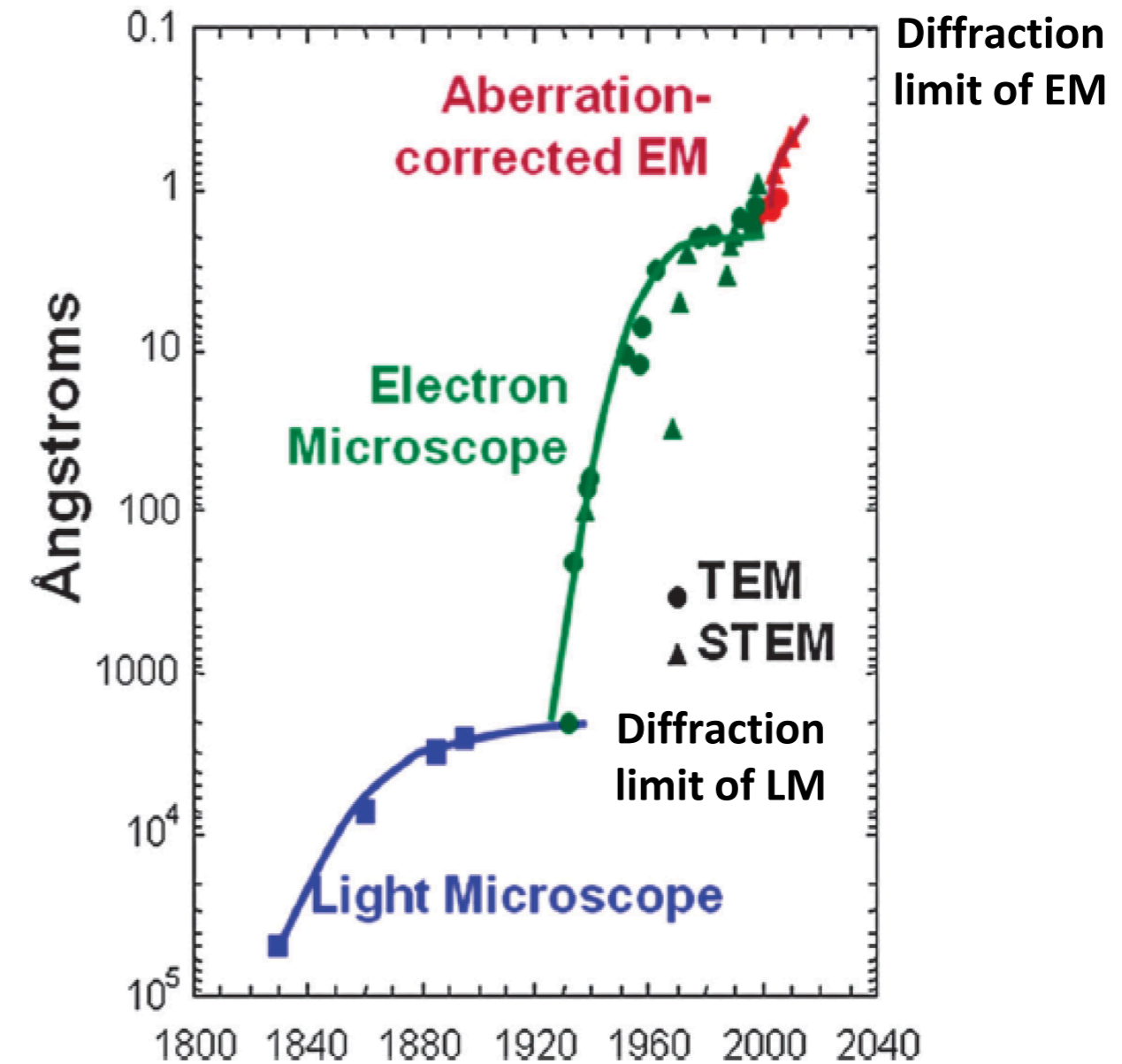
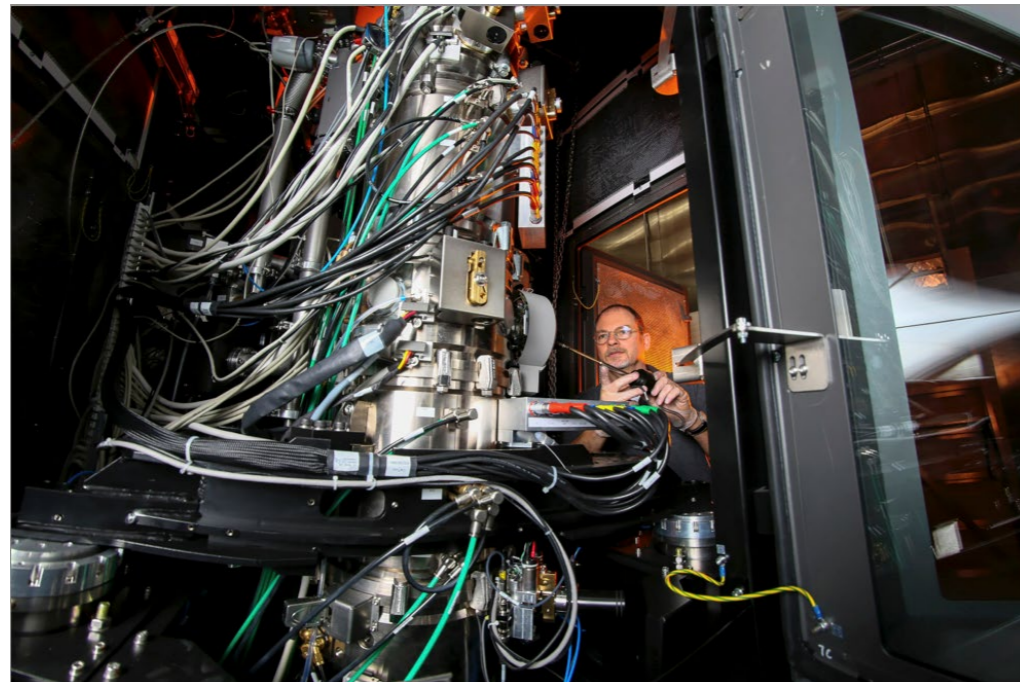
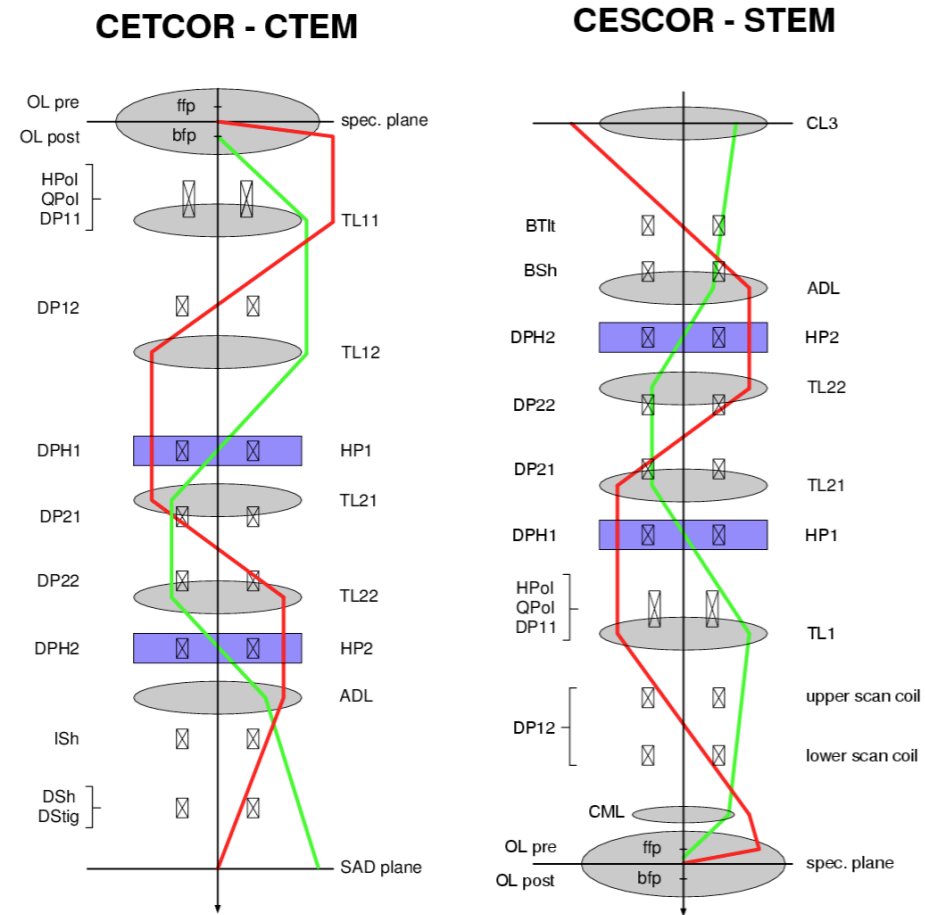
$n = 1$ for vacuum

$\beta = 0.1$ rad given TEM geometry

*** $d = 0.015$ nm

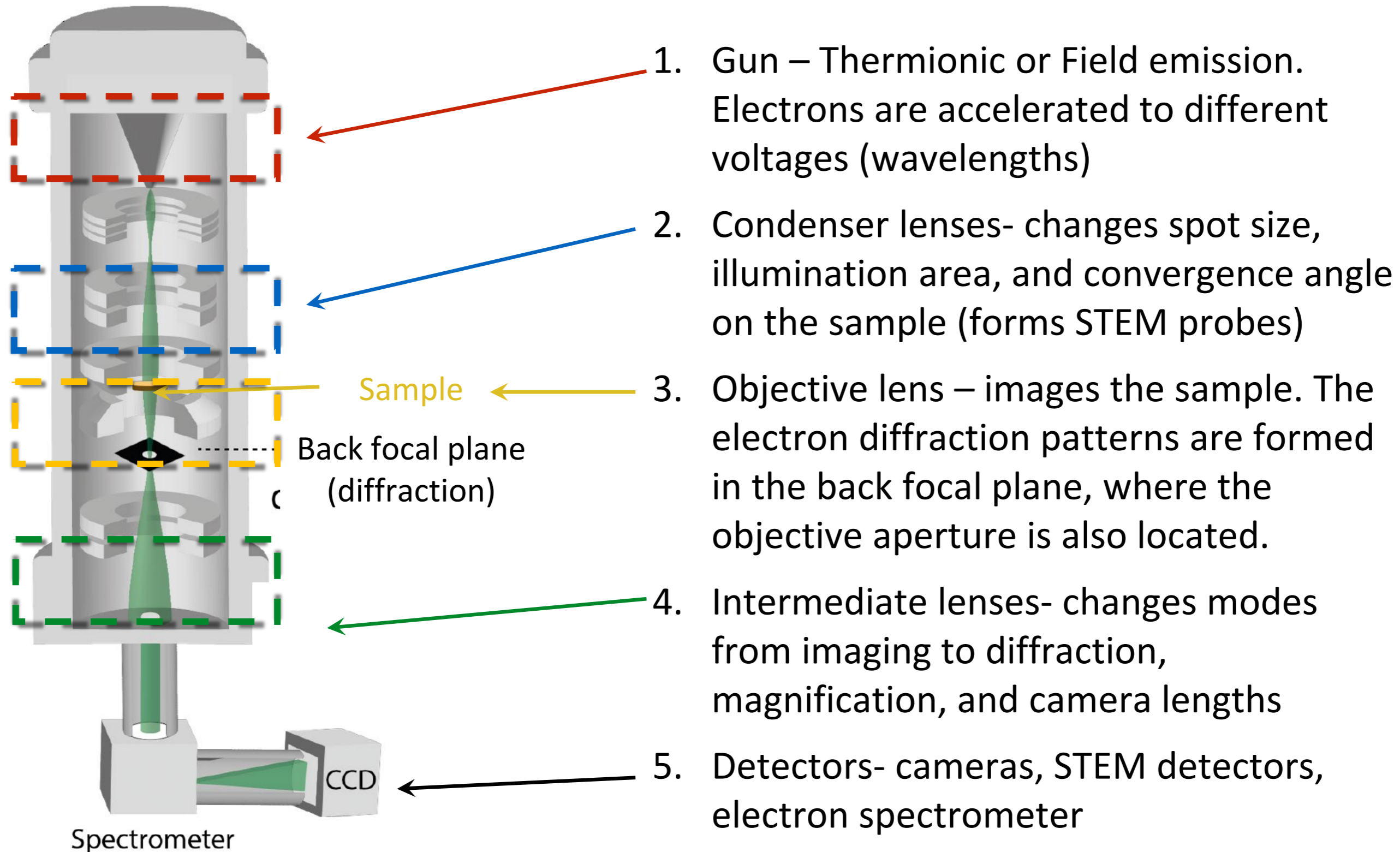
$$d = 0.61 \frac{\lambda}{n \sin \theta} = 0.61 \frac{\lambda}{\beta}$$

Aberration Correction

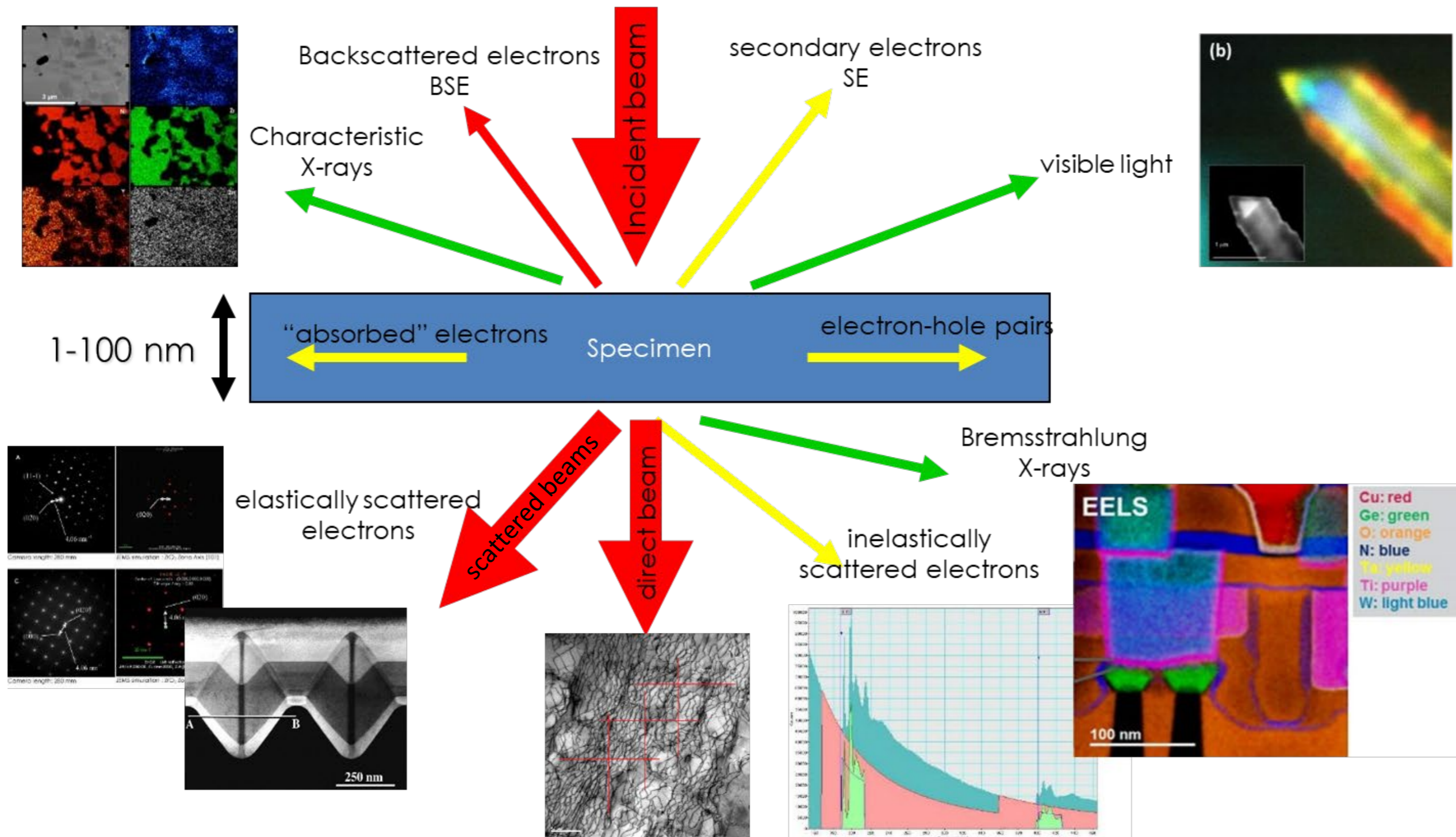


Uncorrected resolution is $\sim 150 \times$ diffraction limit
 Cs-Corrected resolution is $\sim 20 \times$ diffraction limit

Transmission Electron Microscope



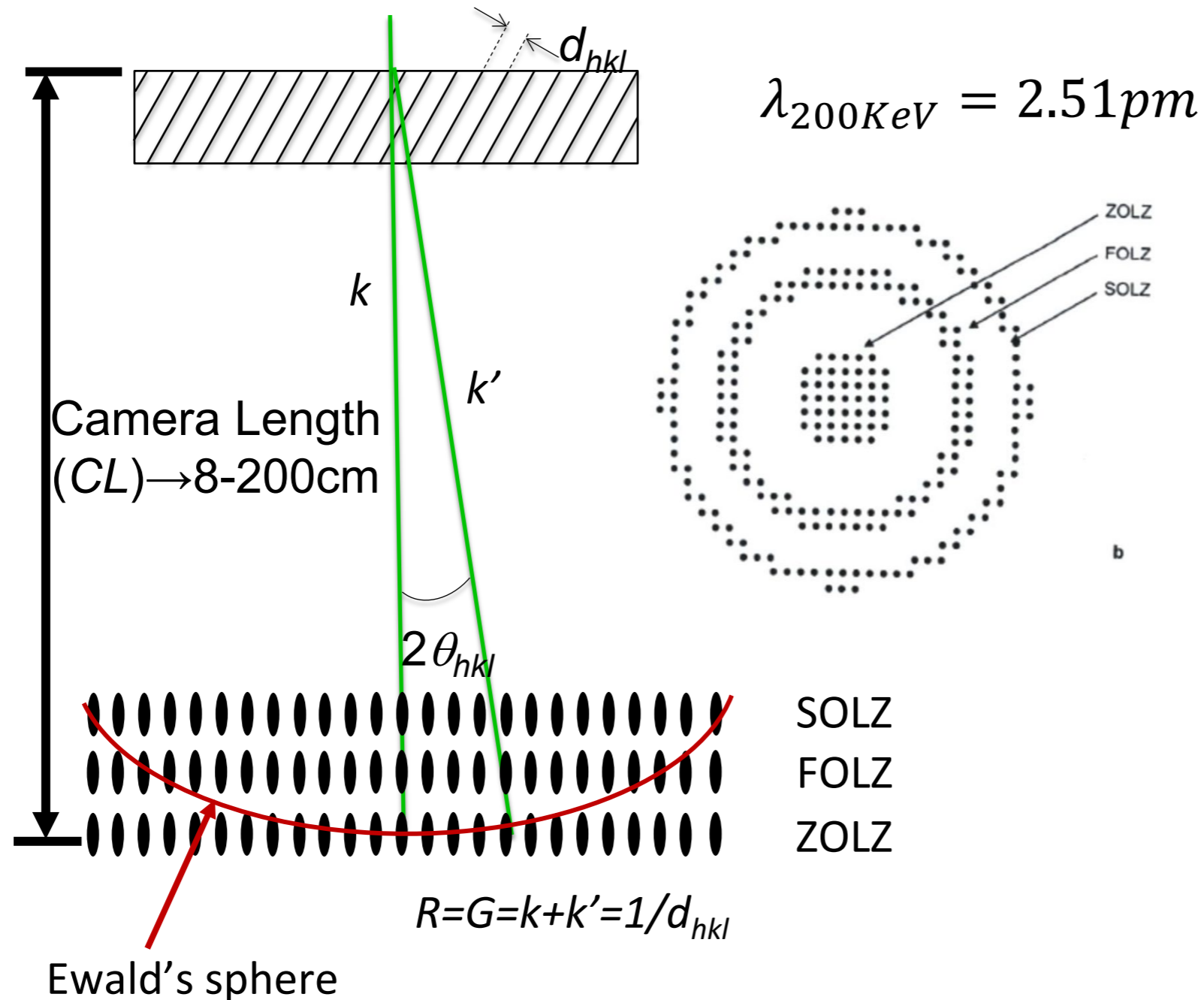
Interaction of high energy electrons with samples



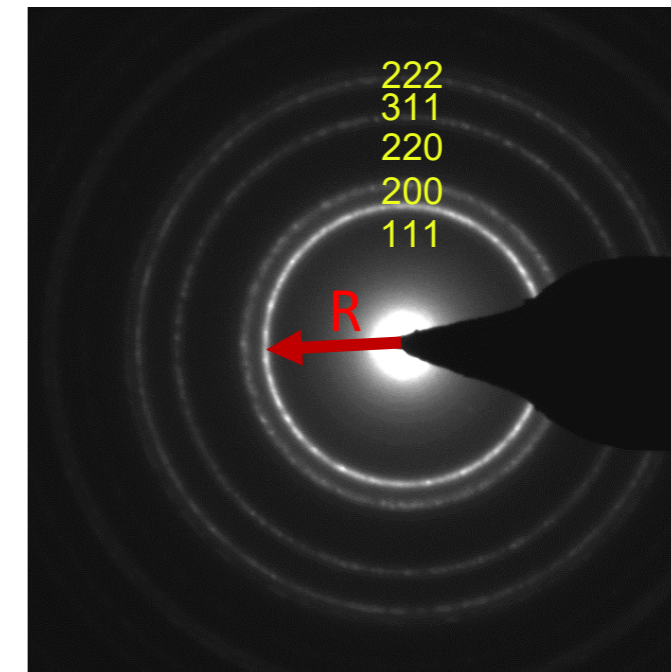
Selected Area Electron Diffraction

$$2d\sin\theta = 2\theta d = n\lambda$$

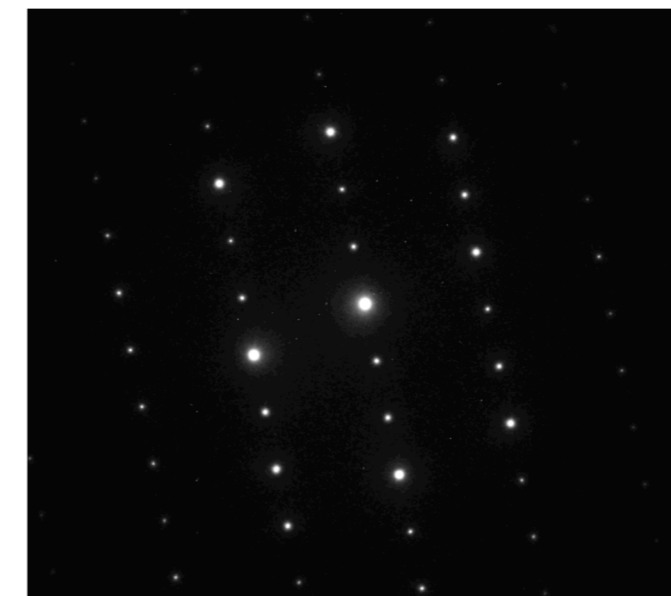
$$R\lambda = 2\theta = R/CL, d_{hkl} = \lambda CL/R$$



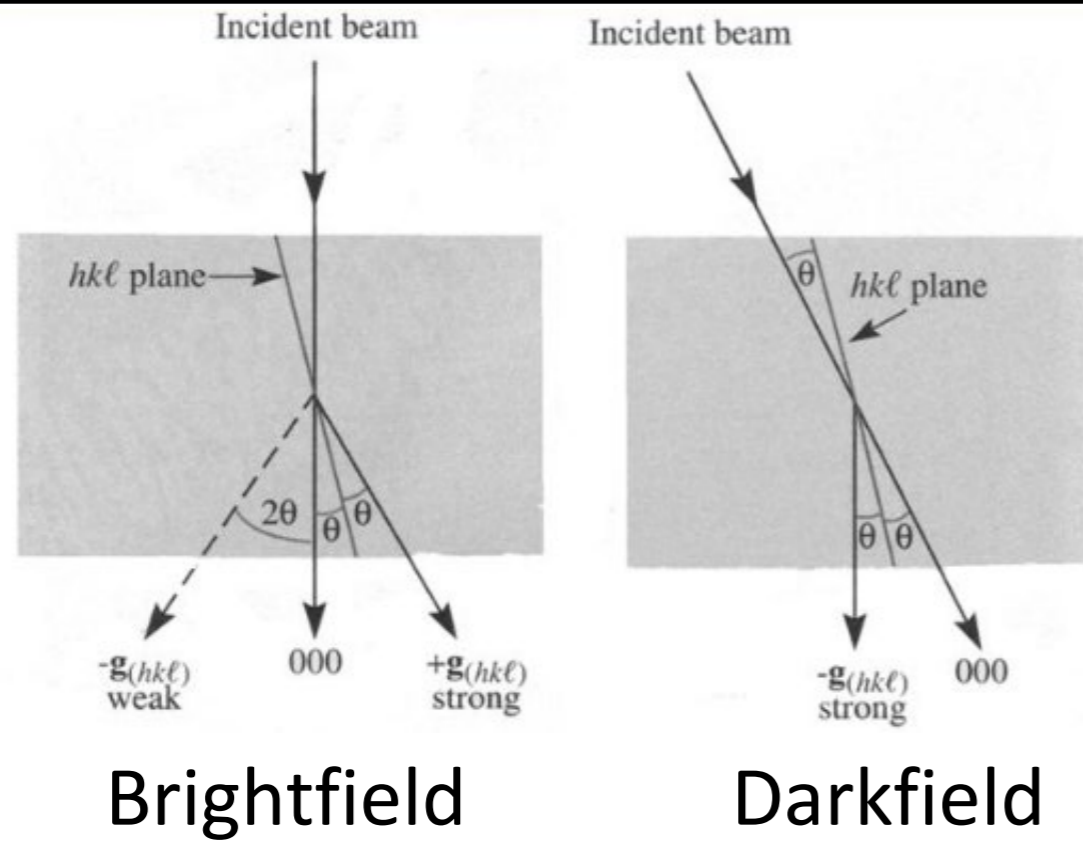
Bragg Diffraction Powder Pattern



Single Crystal Spot Pattern

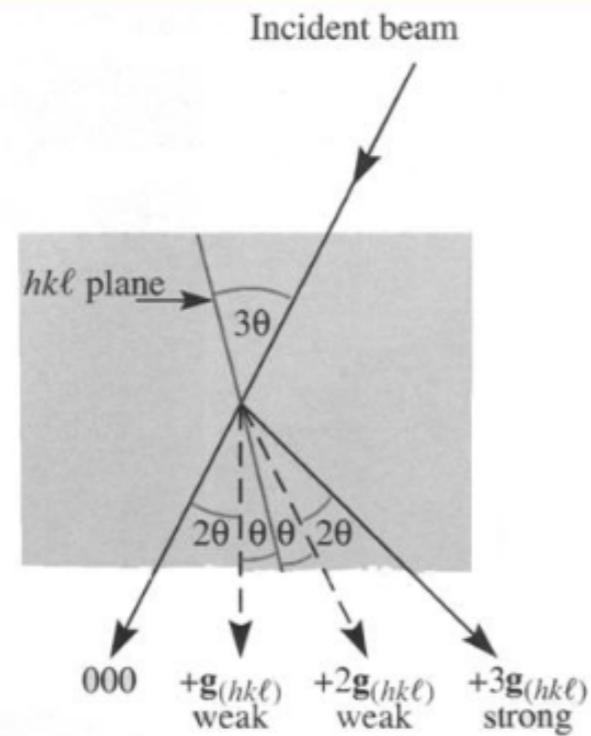


2-Beam Condition

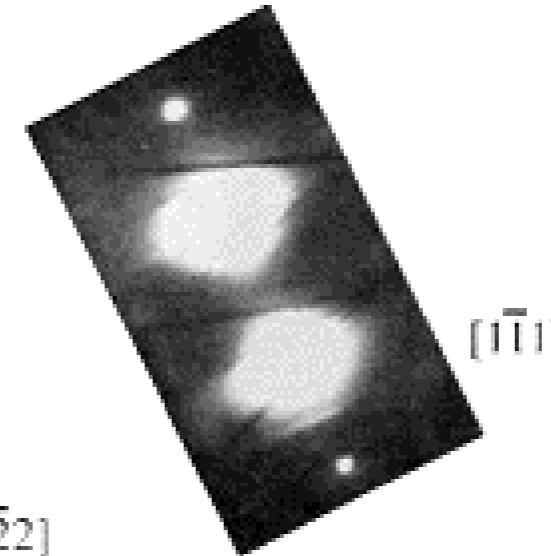
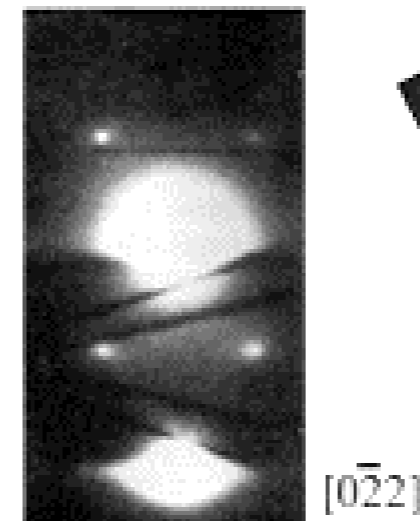
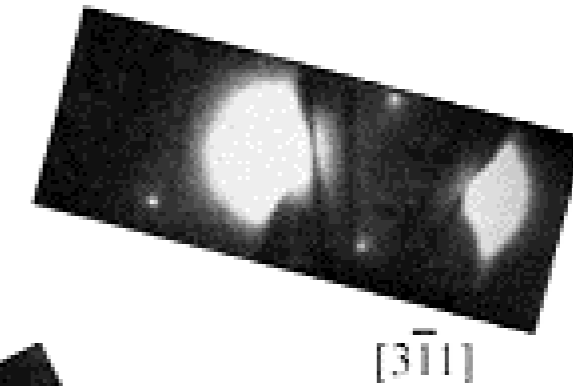
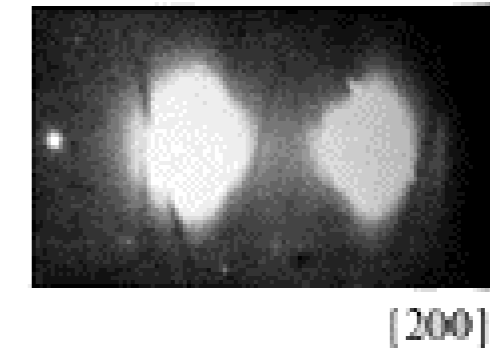
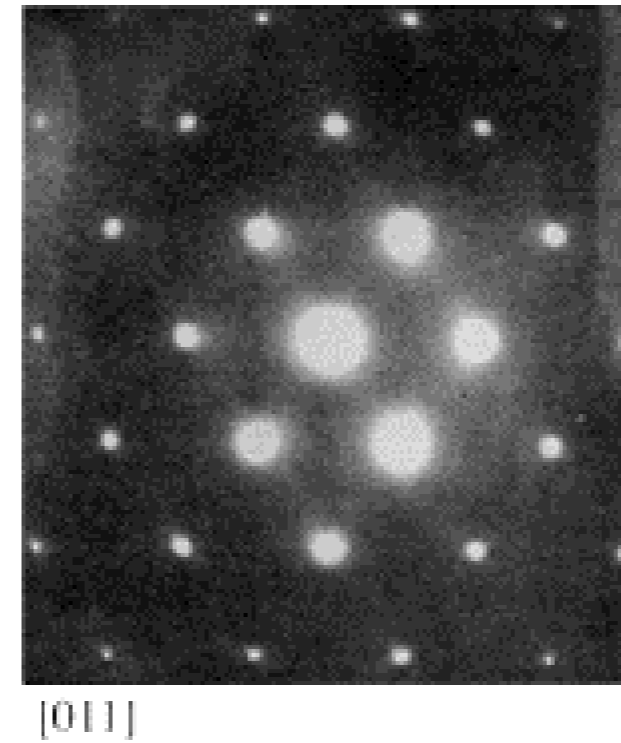


Brightfield

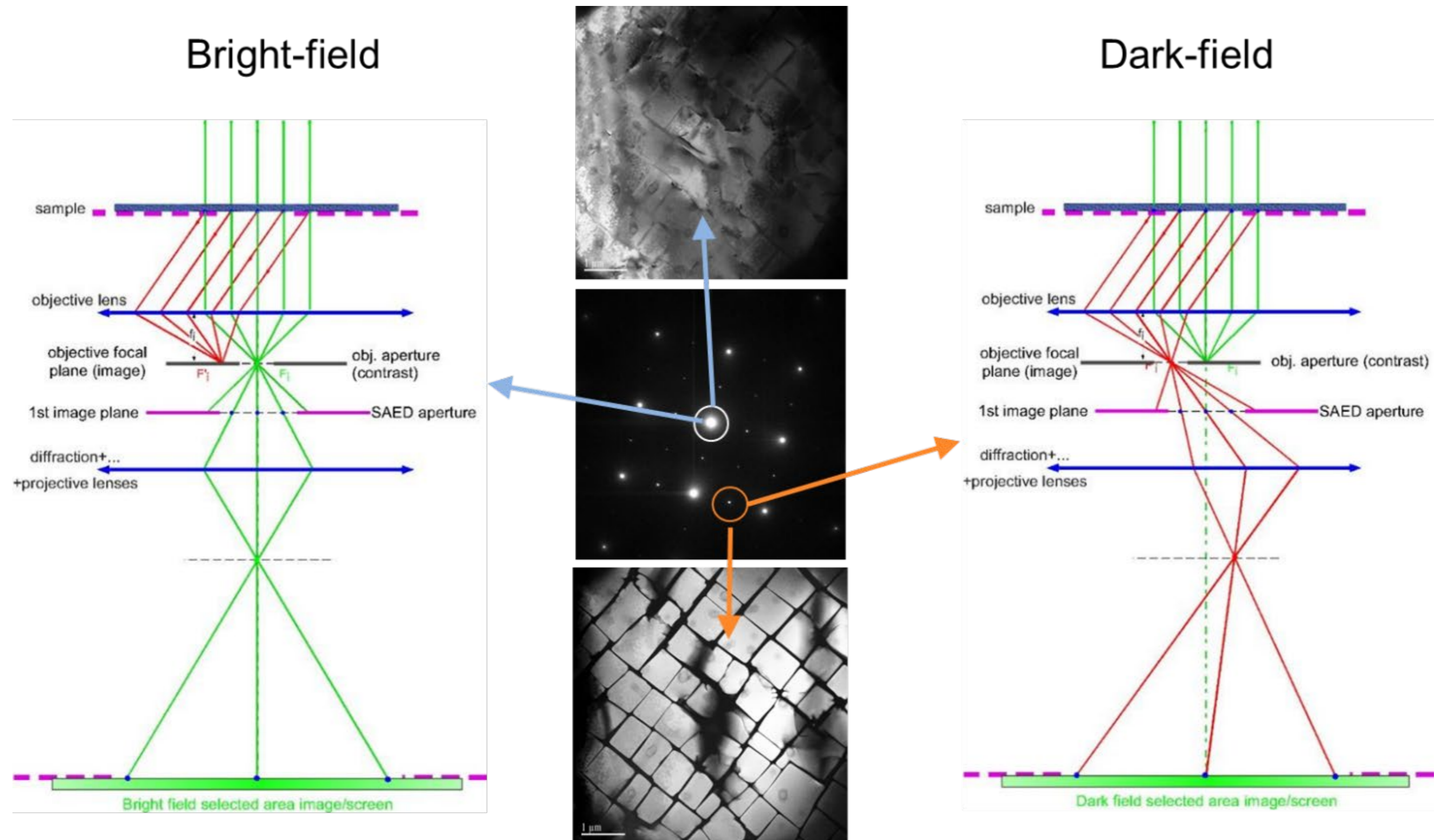
Darkfield



Weak-beam
Darkfield



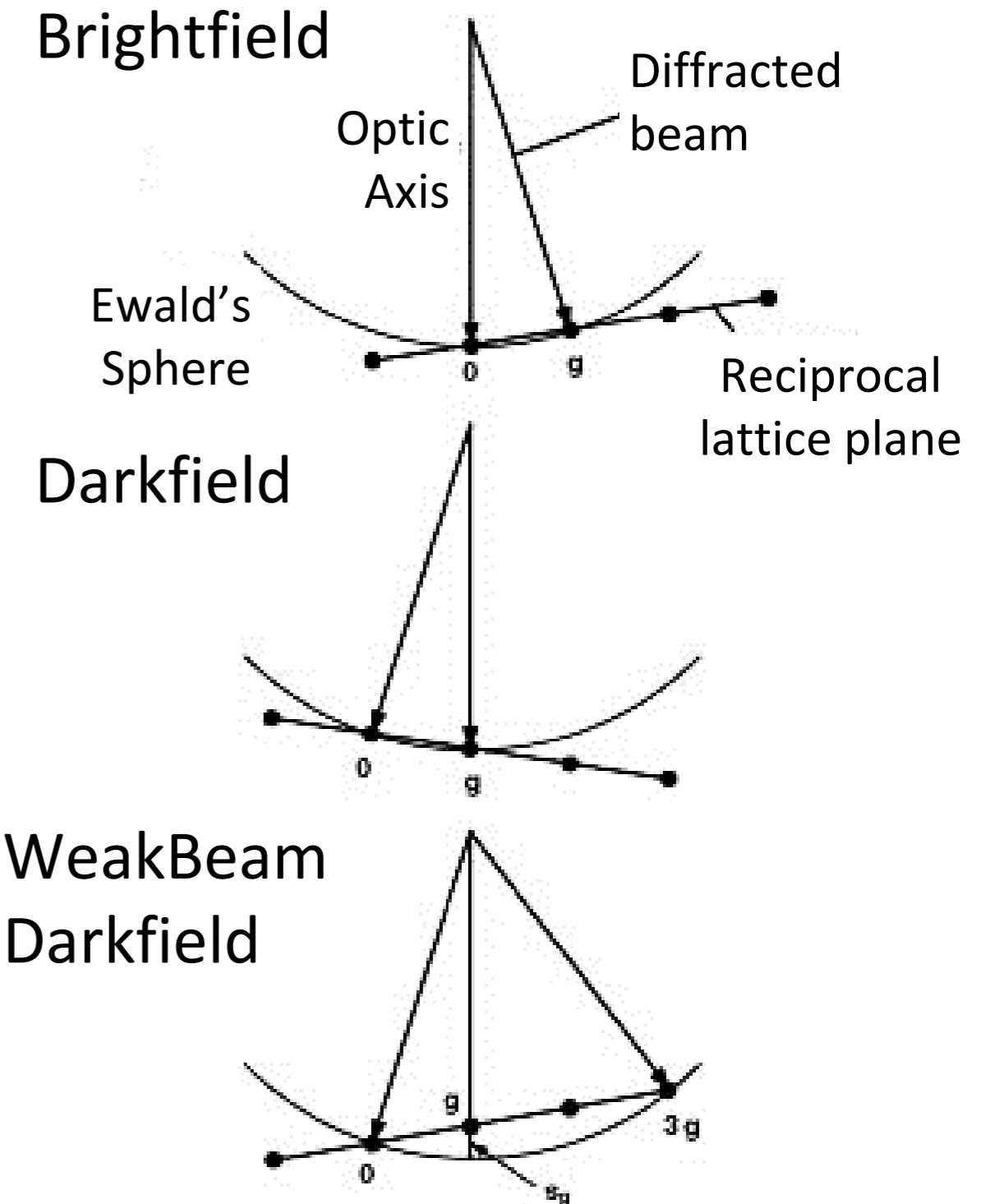
Diffraction Contrast



Dislocation imaging

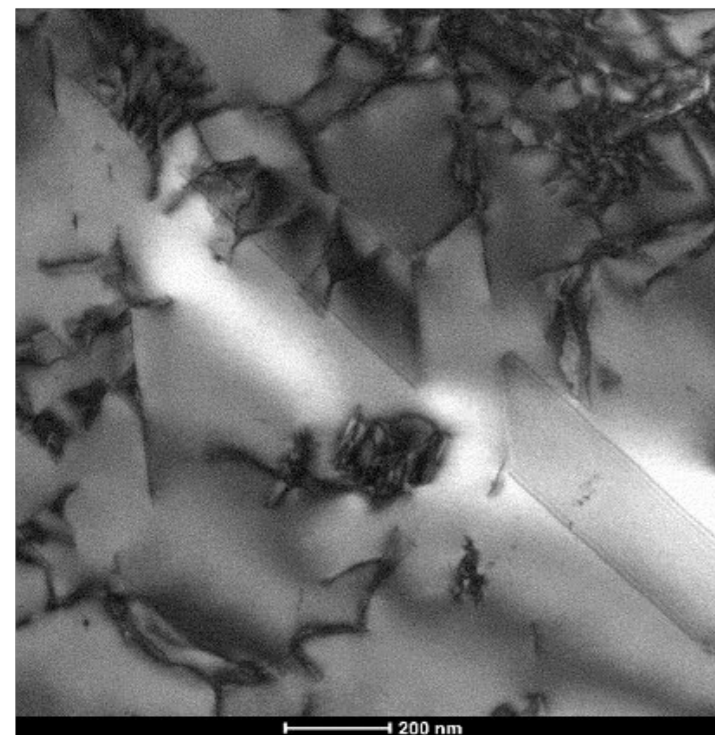
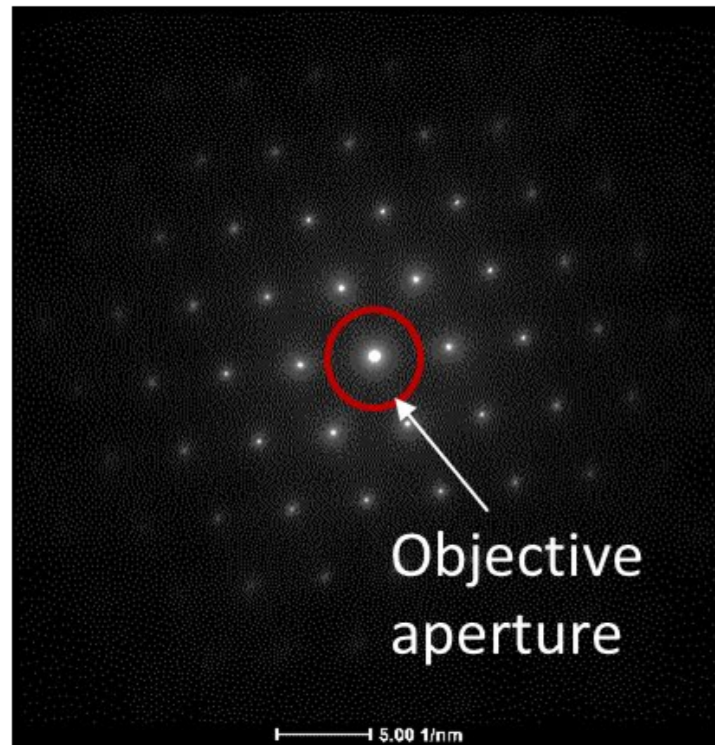
- Strong beam Bright-field or Two beam condition: the sample is first tilted such that g image is excited (Ewald sphere intersects g) and strong in intensity.
- Strong beam Dark field: the image is formed using the excited, high-intensity (g) diffracted beam
- Weak Beam Dark-field (WBDF): the sample is tilted such that the $3g$ and 0 spots are both excited, and the objective aperture is centered on the **WEAK** g spot.

WBDF is useful for imaging defects since the excitation error is small, and defects such as dislocations are better resolved

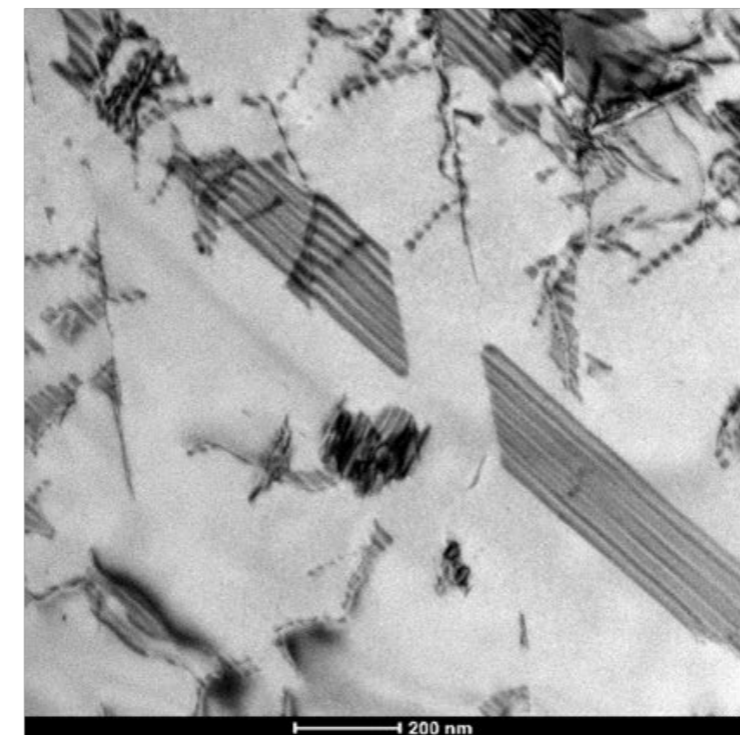
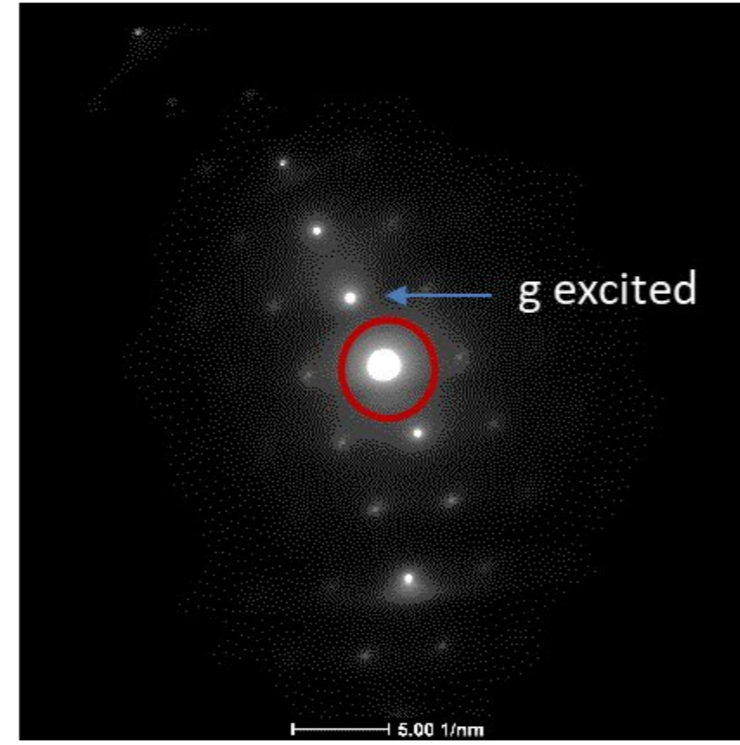


ZA (Kinematical) imaging vs. 2-Beam vs. Weak Beam

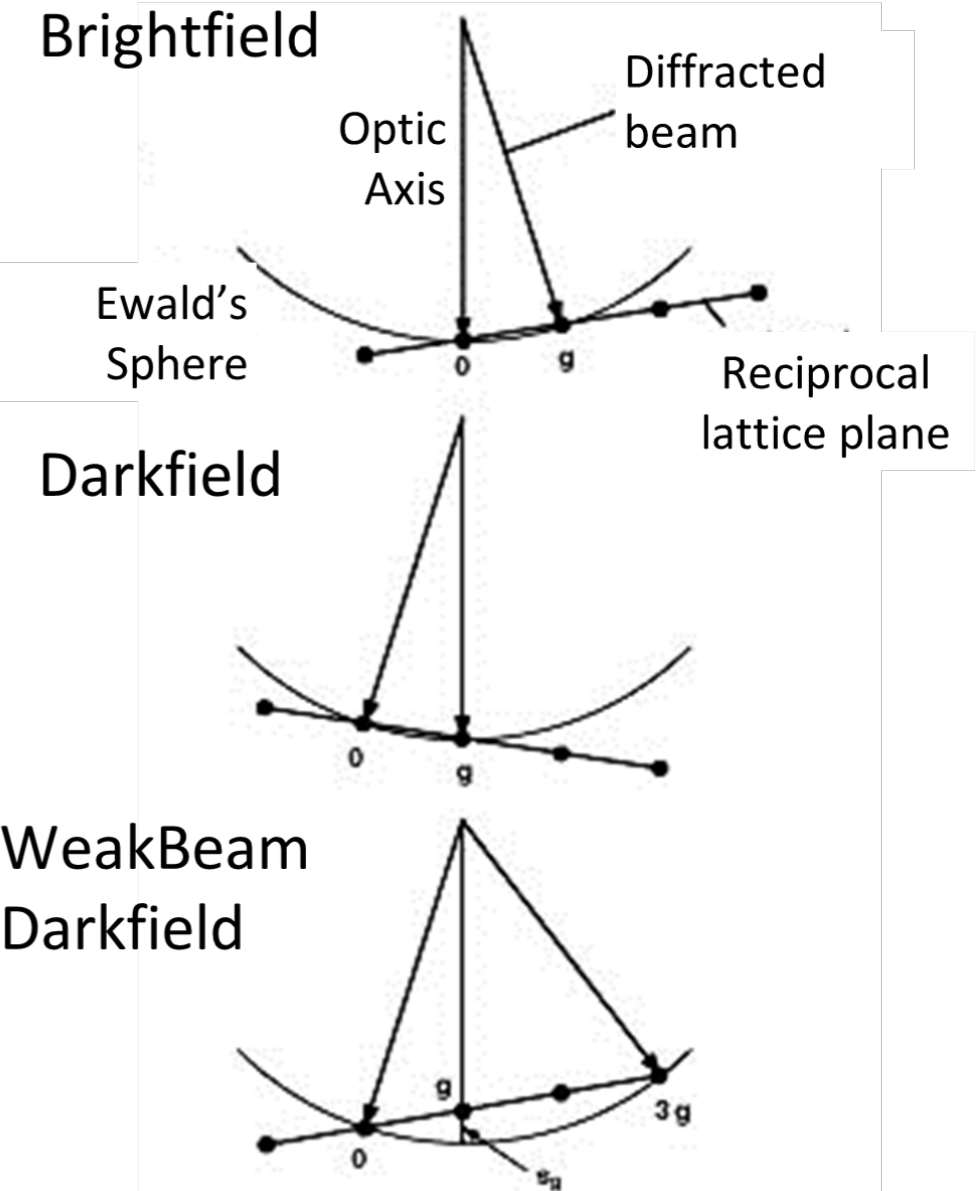
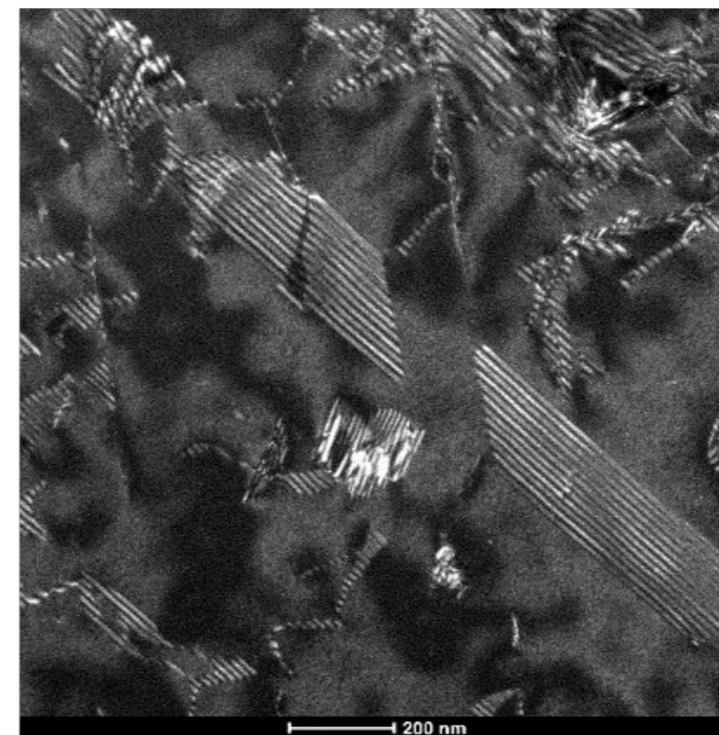
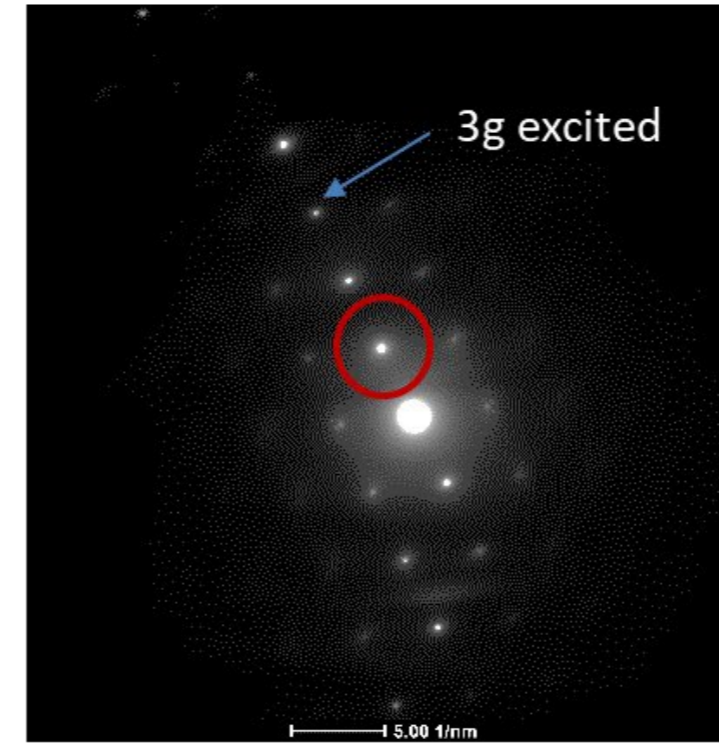
Zone Axis Bright-field



Two Beam Bright-field

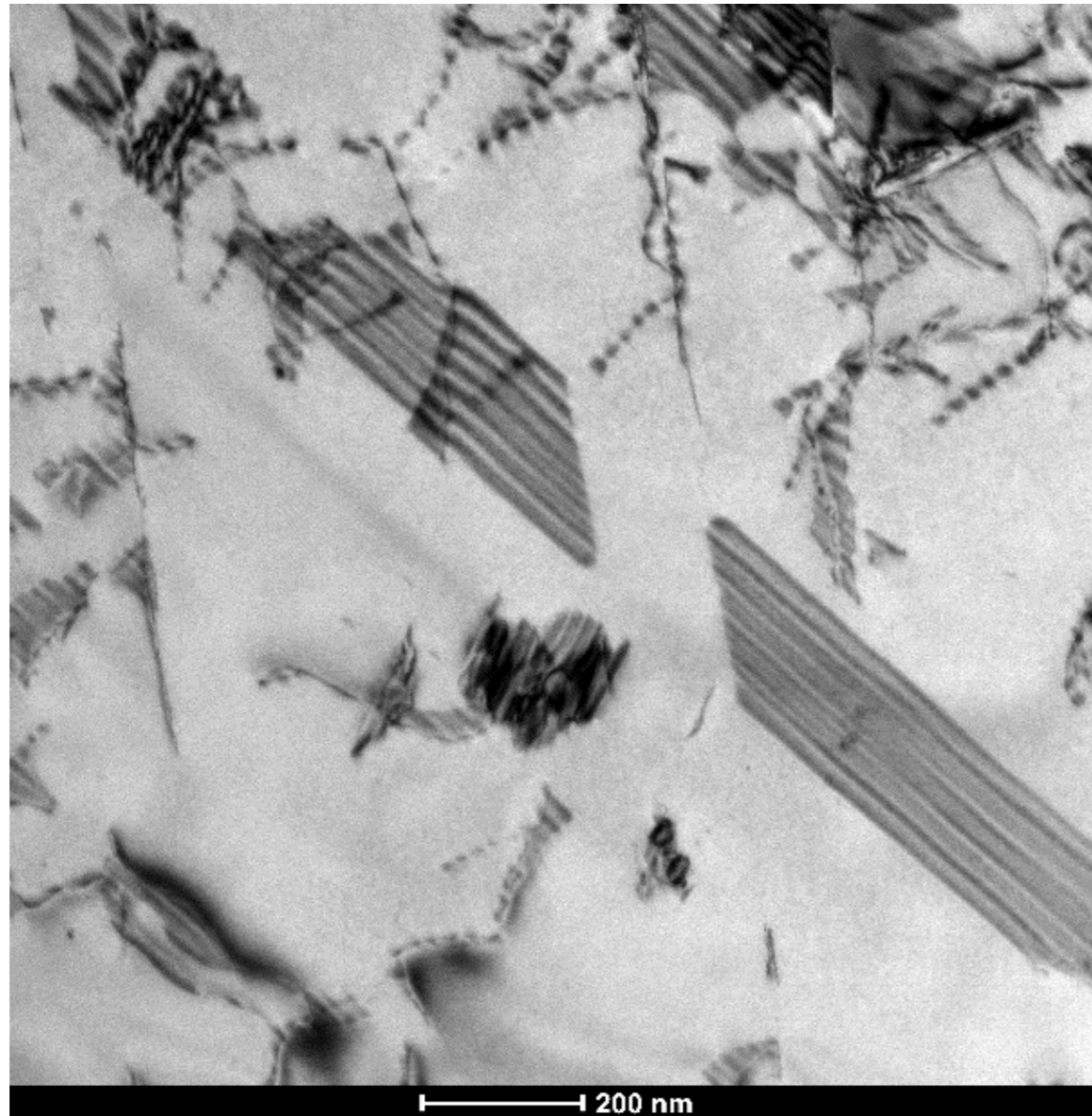


Weak Beam Image

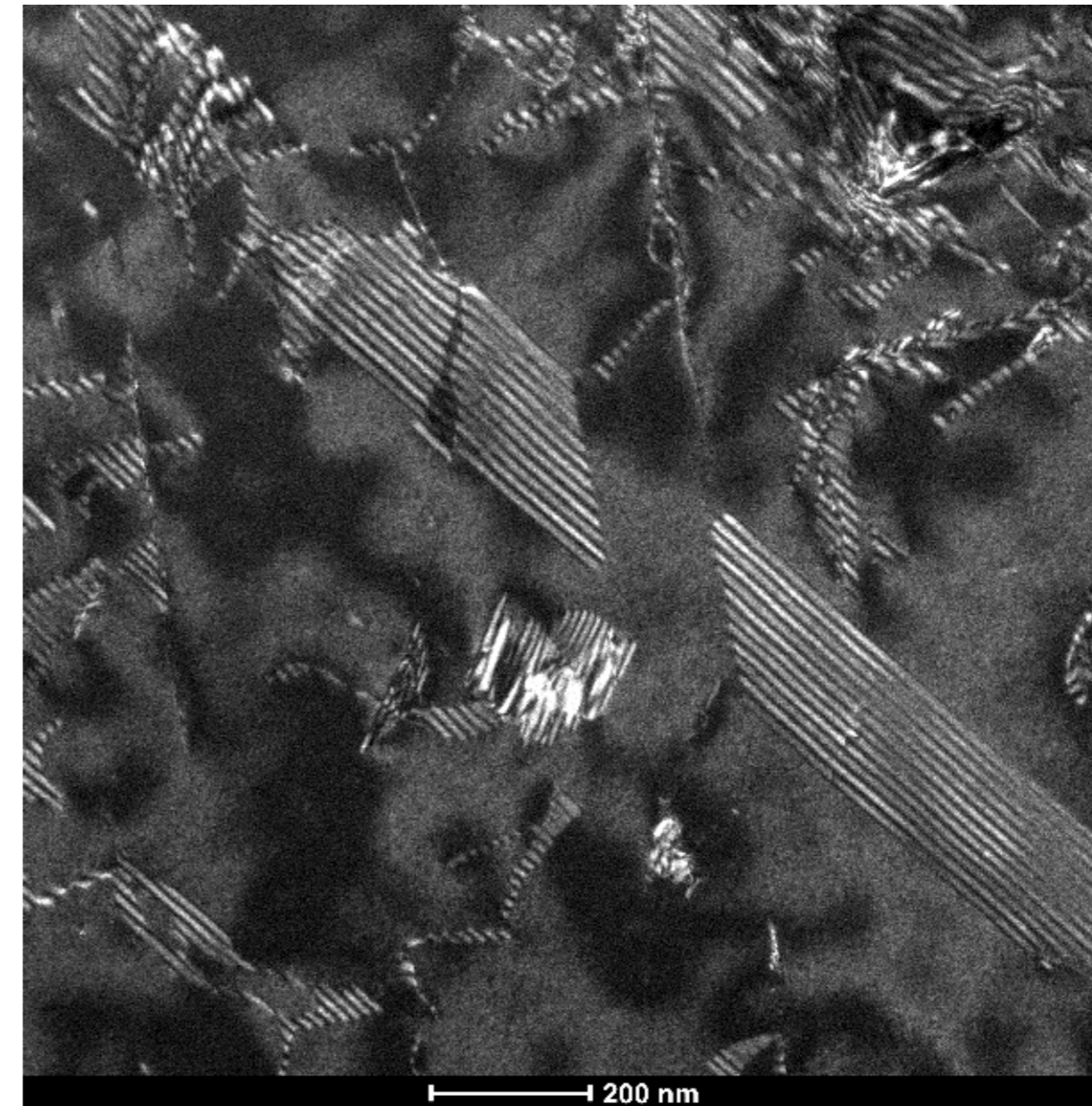


Stacking Faults imaged with Weak Beam

Two Beam Bright-field

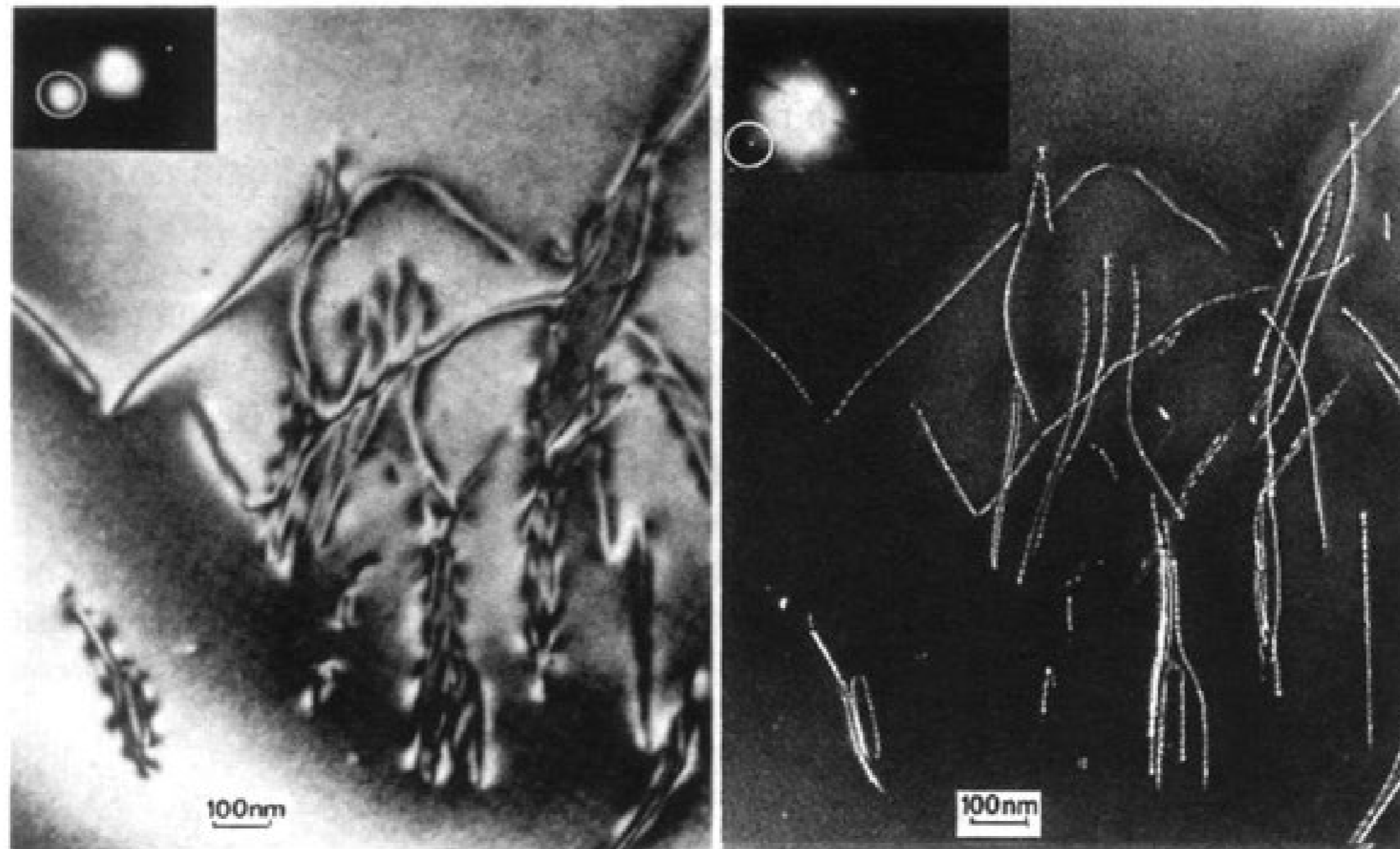


Weak Beam Image



Fringe spacing correlates to partial dislocation separation distances which can be measured clearly in weak beam due to improved contrast and resolution

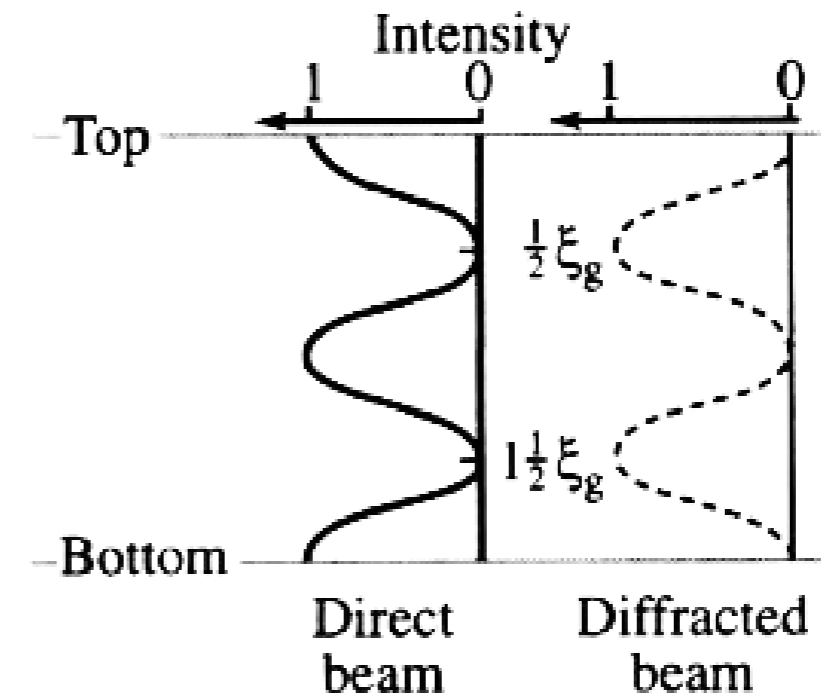
Weak-beam provides $<5\text{nm}$ resolution



Kinematical Diffraction

Assumptions

- Only 2 diffracted beams are considered, direct and one diffracted (aka why we do 2-beam condition)
- Intensity of the diffracted beam is small
- Single scattering event, that is “one cycle” intensity change
- No absorption, i.e., $I_{\text{diffracted}} \ll I_{\text{transmitted}}$



$$I_{diff} = \frac{\sin^2(\pi z s)}{\xi_g s^2}$$

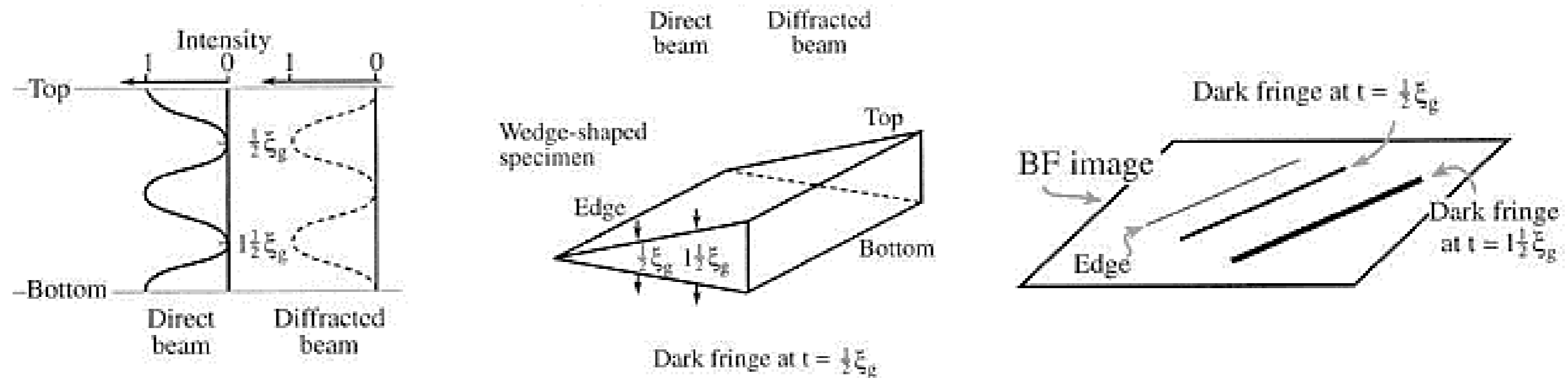
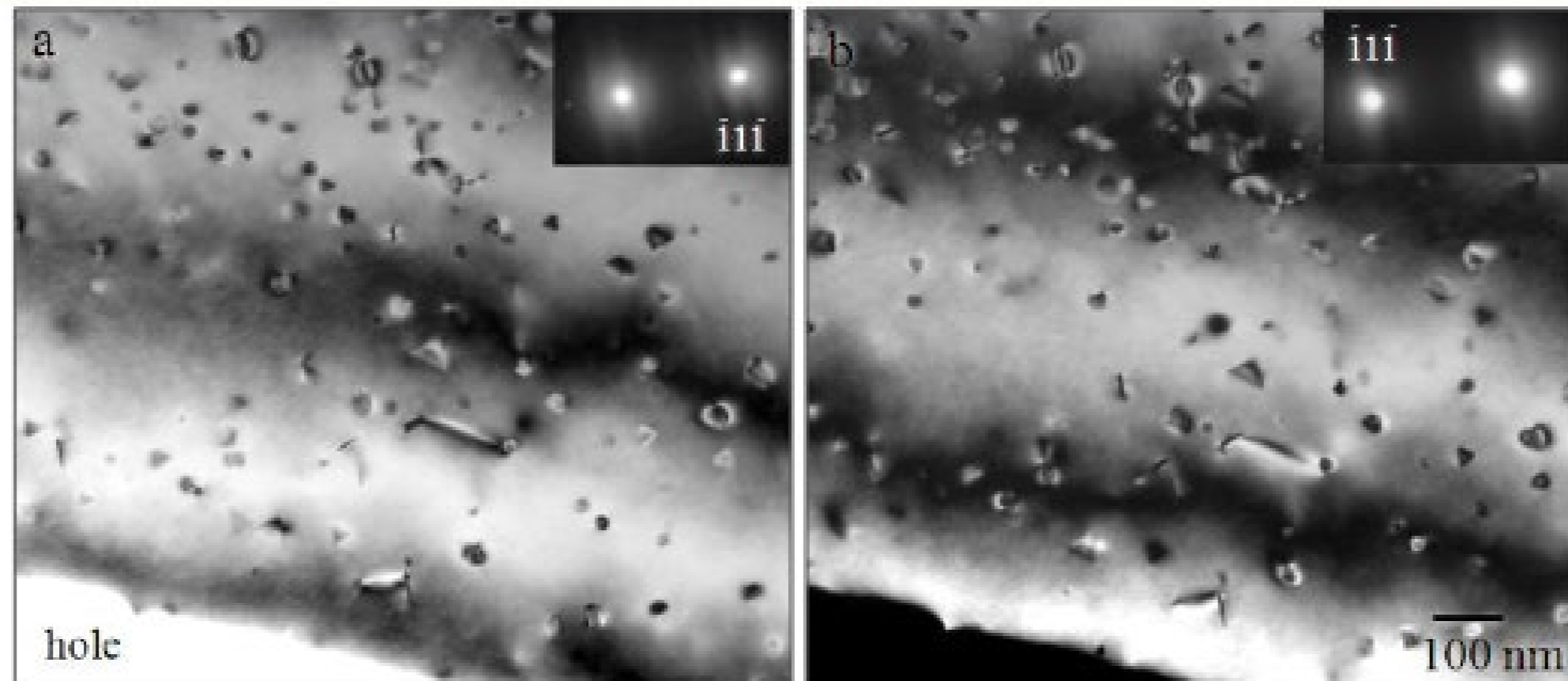
$$I_{trans} = 1 - I_{diff}$$

$$\xi_g = \frac{\pi V_c \cos \theta_B}{\lambda F_g}$$

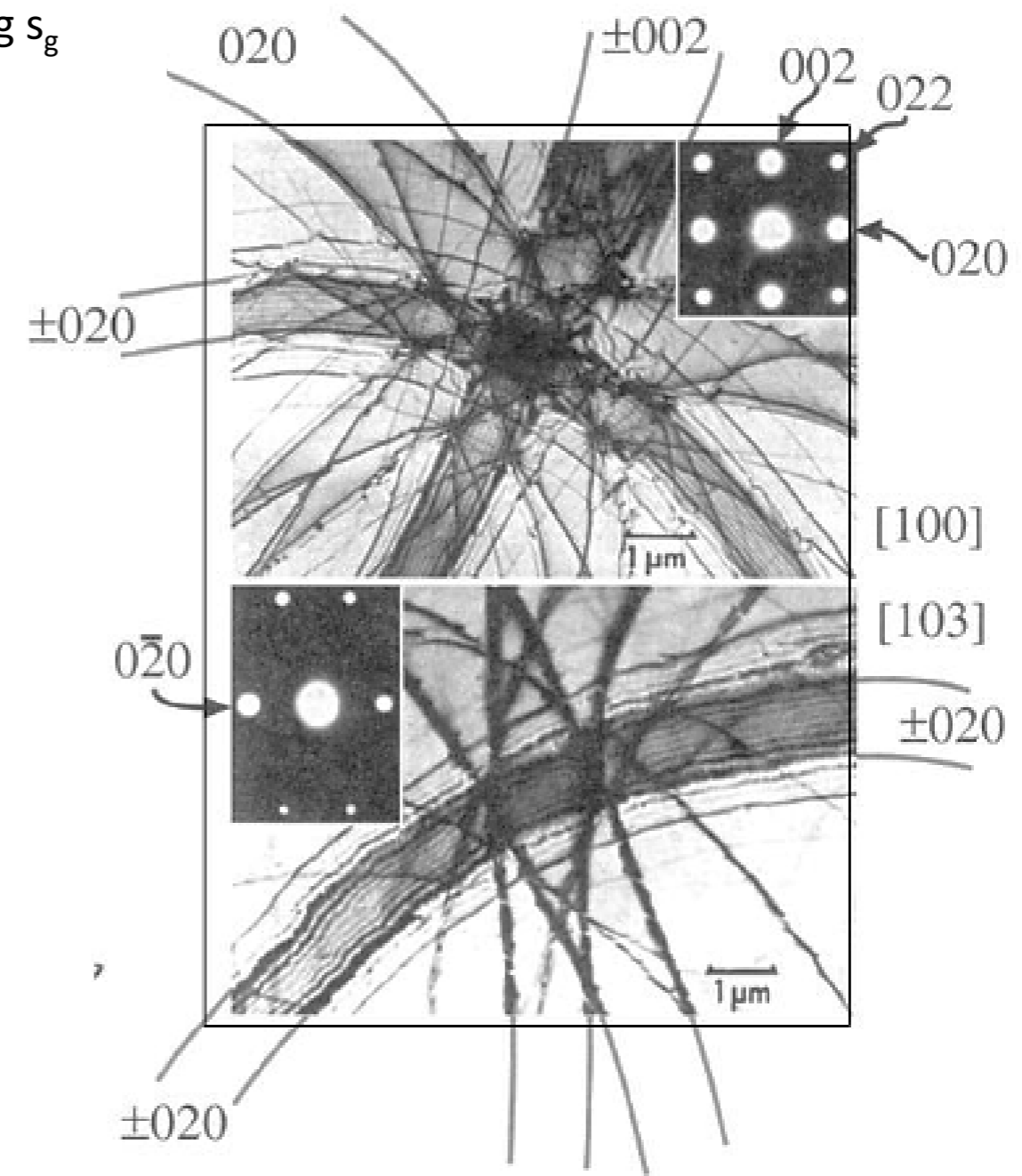
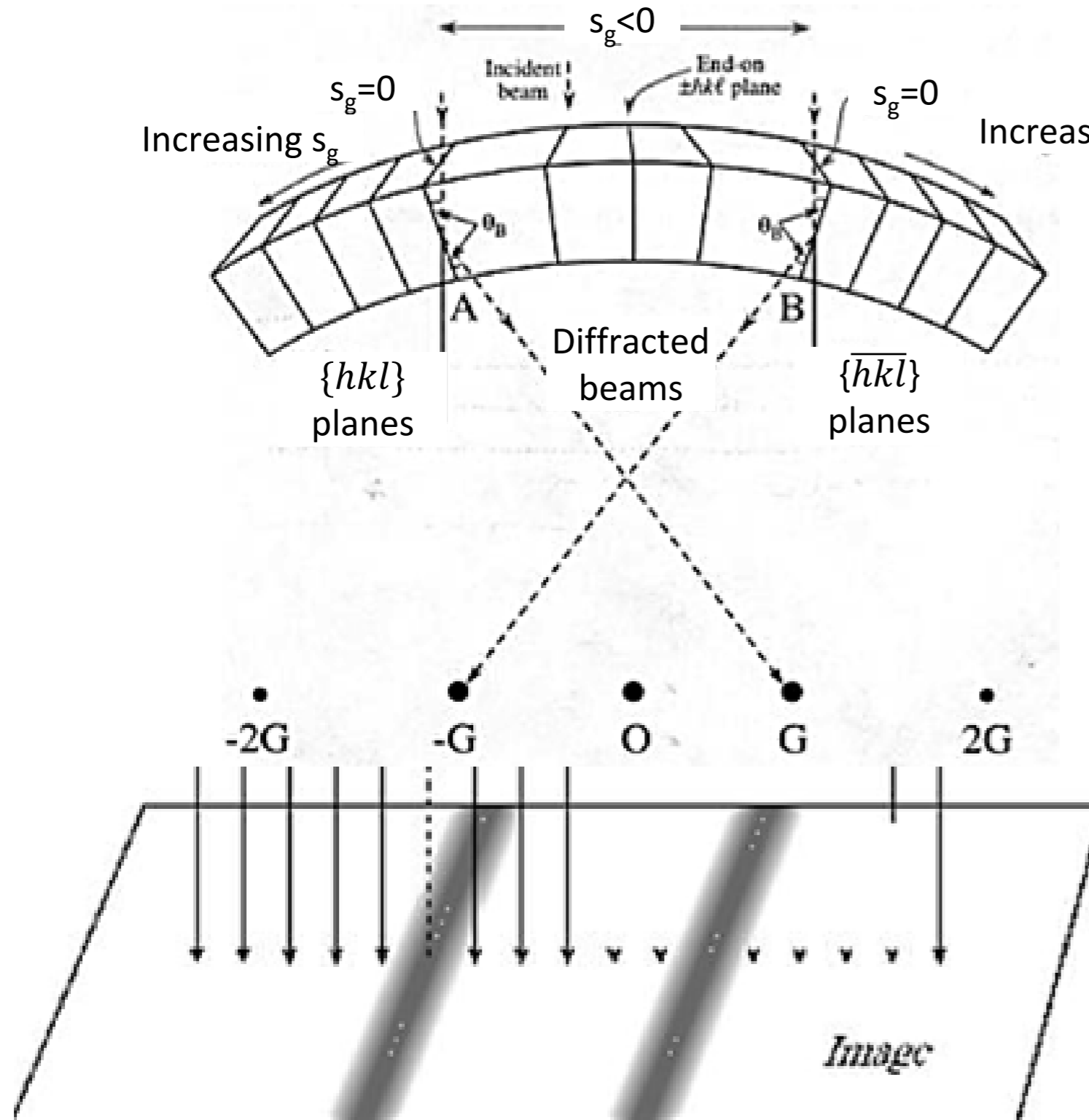
Thickness Fringes

Brightfield

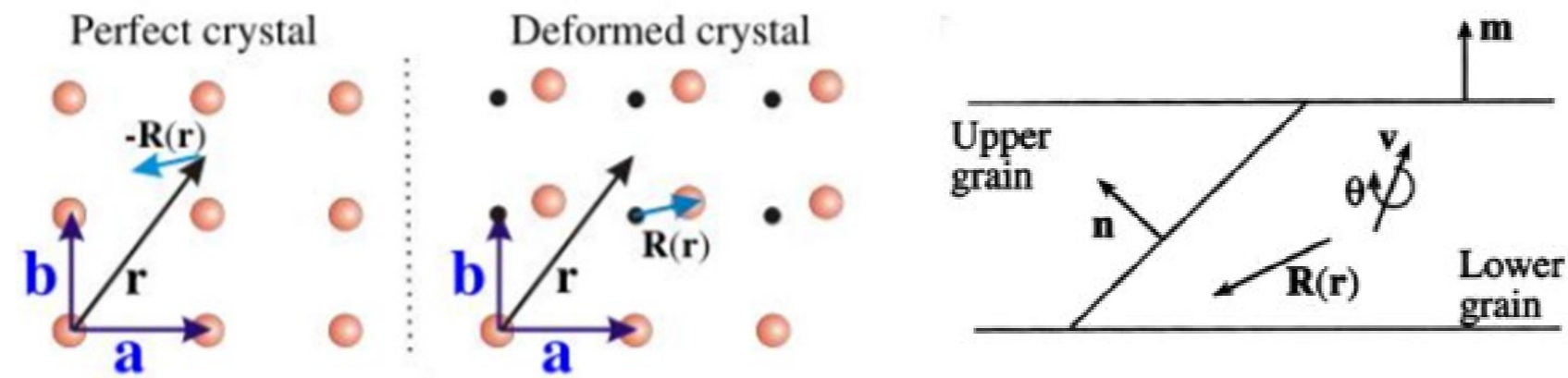
Darkfield



Bend Contours



Kinematic Diffraction in crystals with defects

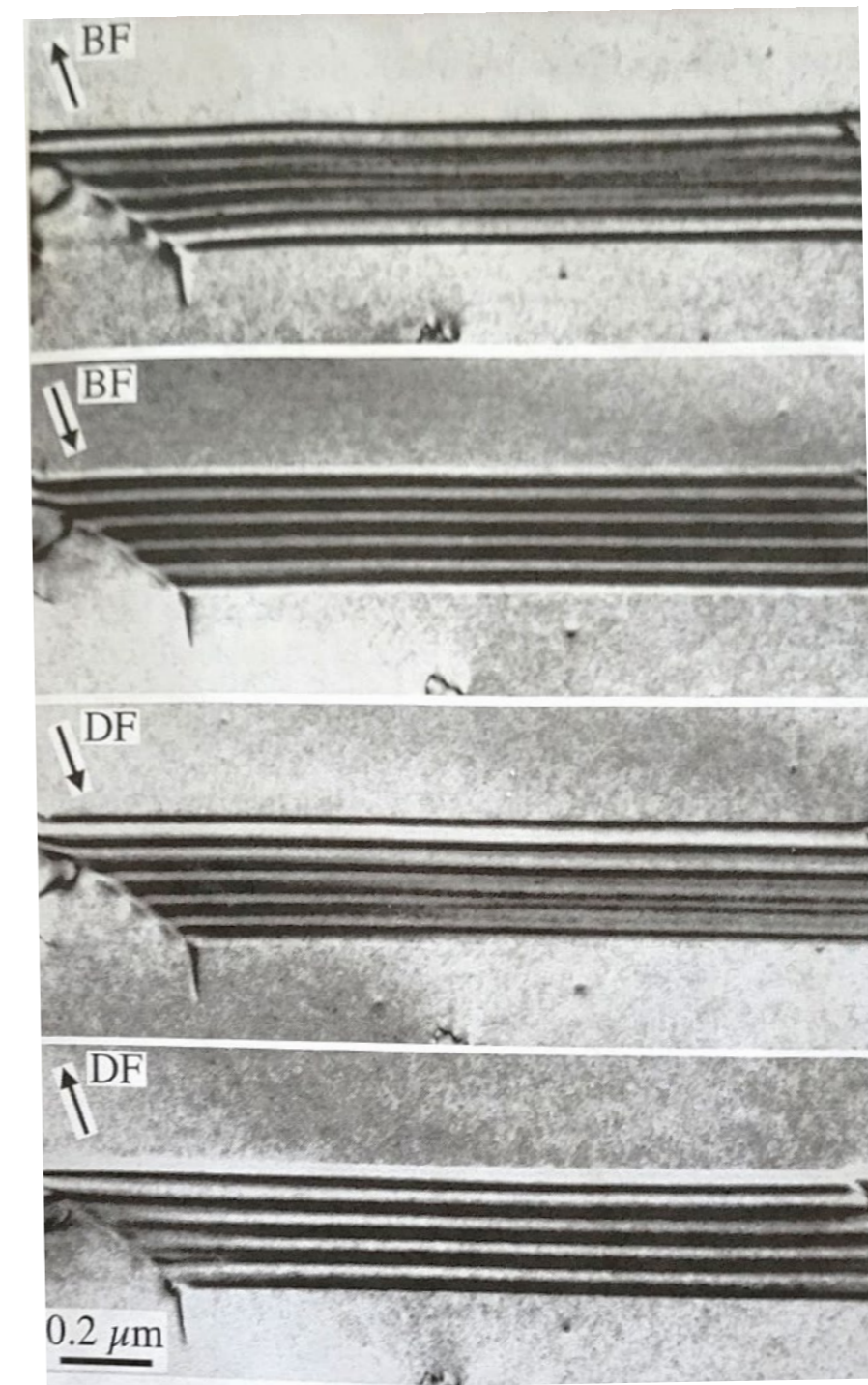


$$V_{def}(r) = \sum_g V_g e^{2\pi i \mathbf{g} \cdot [\mathbf{r} - \mathbf{R}(\mathbf{r})]}$$

Translations and rotations between two crystals produce fringes in the images

- Stacking Faults
- Grain boundaries
- Translation boundaries
- Phase boundaries
- Stepped Surfaces

Electron wave has different amplitude and phase in each crystal resulting in constructive –destructive interference and fringe patterns



Howie Whelan Equations

$$V(\mathbf{r}) = \sum_{\mathbf{g}} V_{\mathbf{g}} e^{2\pi i \mathbf{g} \cdot \mathbf{r}}$$

Potential of perfect crystal

$$A_{cell} = \frac{e^{2\pi i \mathbf{k} \cdot \mathbf{r}}}{r} F(\theta)$$

Electron scattering amplitude from a unit cell

$$\phi_{\mathbf{g}} = \frac{\pi a i}{\xi_{\mathbf{g}}} e^{2\pi i \mathbf{K} \cdot \mathbf{r}_a} e^{2\pi i \mathbf{k}_{\mathbf{g}} \cdot \mathbf{r}}$$

Scattering amplitude of a diffracted beam (solved using Schrödinger's eqn.)

$$\Psi_T = \phi_0 e^{2\pi i \mathbf{k}_0 \cdot \mathbf{r}} + \phi_{g1} e^{2\pi i \mathbf{k}_{g1} \cdot \mathbf{r}} +$$

$$\phi_{g2} e^{2\pi i \mathbf{k}_{g2} \cdot \mathbf{r}} + \phi_{g3} e^{2\pi i \mathbf{k}_{g3} \cdot \mathbf{r}} \dots$$

Total wavefunction
2-beam condition

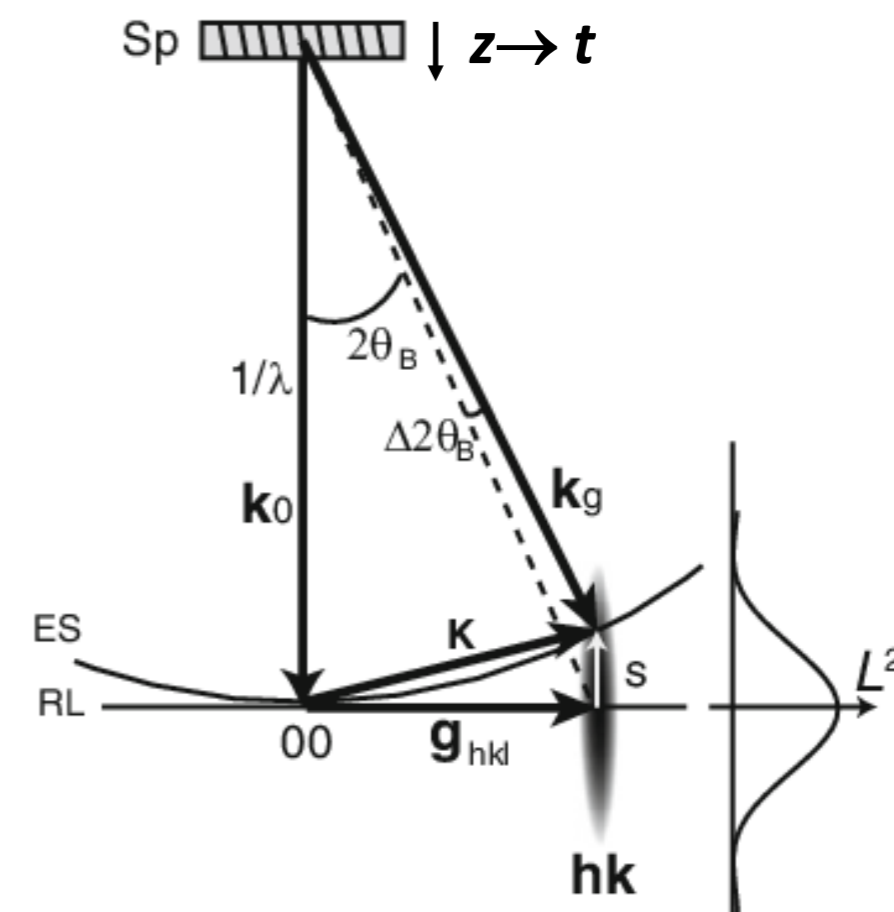
$$\phi_0 = C_0 e^{2\pi i \gamma z},$$

$$\phi_{\mathbf{g}} = 2\xi_{\mathbf{g}} \gamma C_0 e^{2\pi i \gamma z}$$

Scattering amplitudes in terms of γ phase, and \mathbf{r} and \mathbf{s} are parallel to \mathbf{z}

$$I_{\mathbf{g}} = |\phi_{\mathbf{g}}|^2$$

Solving the Bloch Wave equations gives I_{diff}



Extinction Distance

$$\xi_{\mathbf{g}} = \frac{\pi V_c \cos \theta_B}{\lambda F_{\mathbf{g}}}$$

Diffracted Intensity

$$I_{\mathbf{g}} = \frac{\sin^2(\pi t s)}{\xi_{\mathbf{g}} s^2}$$

$$I_0 = 1 - I_{\mathbf{g}}$$

Howie Whelan (Darwin) Equations

DYNAMICAL DIFFRACTION

The amplitudes of ϕ_g and ϕ_o are coupled and change with propagation in the sample.

$$d\phi_o = \left\{ \frac{\pi i}{\xi_g} \phi_g e^{-2\pi i \mathbf{K} \cdot \mathbf{r}} + \frac{\pi i}{\xi_o} \phi_o \right\} dz \text{ and } d\phi_g = \left\{ \frac{\pi i}{\xi_g} \phi_o e^{2\pi i \mathbf{K} \cdot \mathbf{r}} + \frac{\pi i}{\xi_o} \phi_g \right\} dz$$

HOWIE-WHELAN EQUATIONS (perfect crystal)

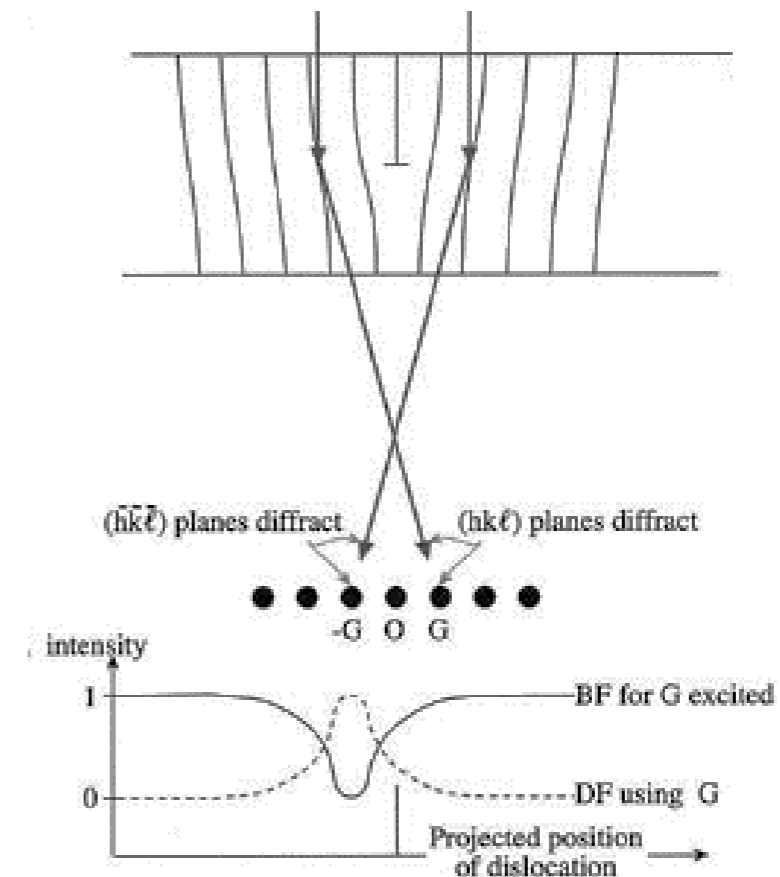
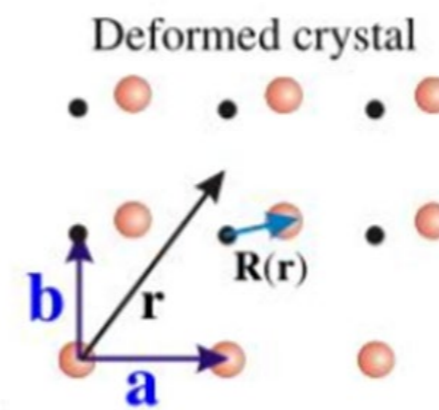
$$\frac{d\phi_o}{dz} = \left\{ \frac{\pi i}{\xi_g} \phi_g e^{2\pi i s z} + \frac{\pi i}{\xi_o} \phi_o \right\} \text{ and } \frac{d\phi_g}{dz} = \left\{ \frac{\pi i}{\xi_g} \phi_o e^{-2\pi i s z} + \frac{\pi i}{\xi_o} \phi_g \right\}, s z = \mathbf{s} \cdot \mathbf{r}$$

HOWIE-WHELAN EQUATIONS for DEFECTS

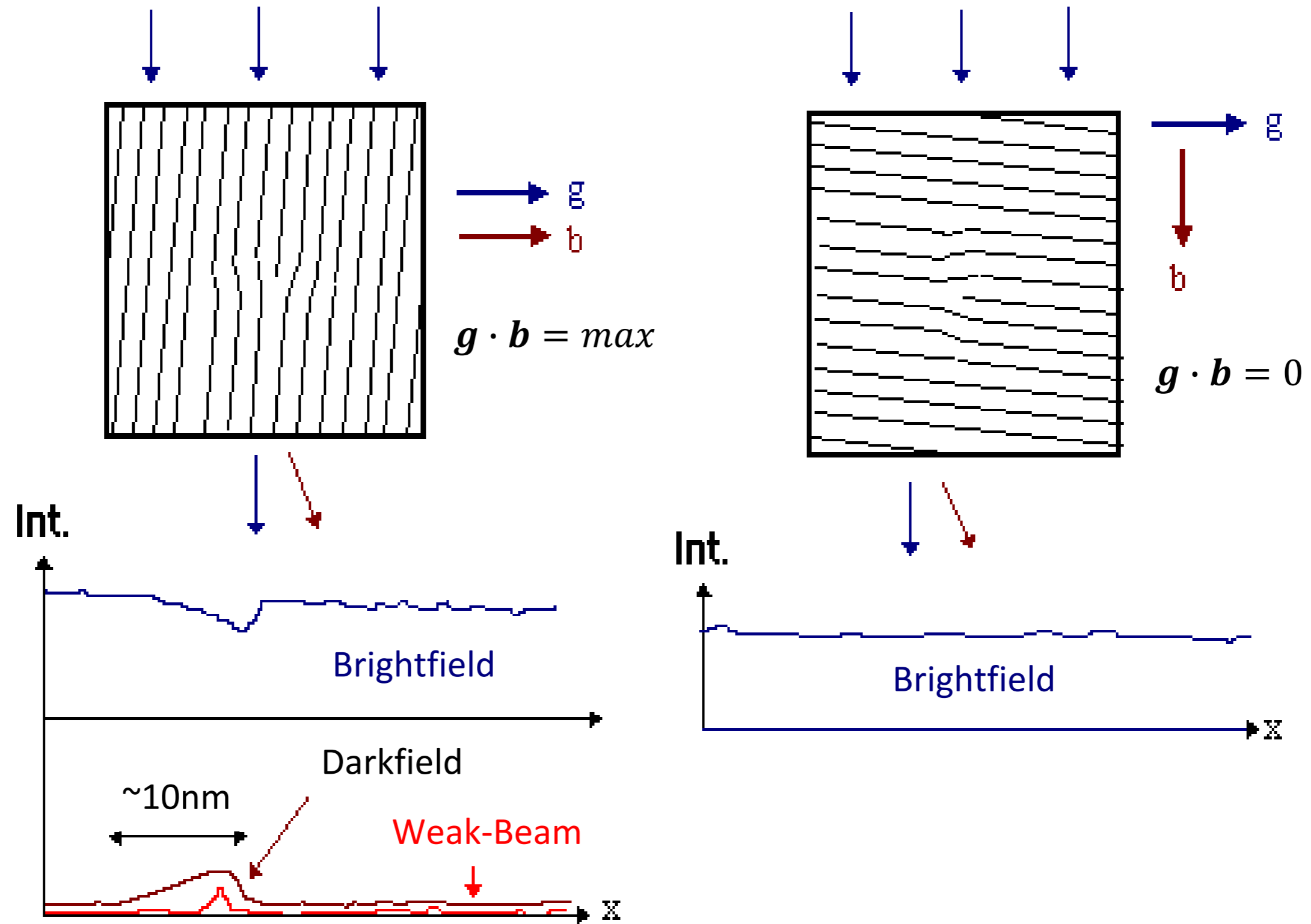
$$\phi_o(z)' = \phi_o \exp\left(\frac{-\pi i z}{\xi_o}\right)$$

$$\phi_g(z)' = \phi_g \exp\left(2\pi i s z - \frac{\pi i z}{\xi_o} + 2\pi i \mathbf{g} \cdot \mathbf{R}(\mathbf{r})\right)$$

$$\frac{d\phi_g}{dz} = \frac{\pi i}{\xi_g} \phi_o(z)' + 2\pi i s_R \phi_g(z)' \text{ and } s_R = s + \mathbf{g} \cdot \frac{d\mathbf{R}(\mathbf{r})}{dz}$$



Strain Contrast for Dislocations



Invisibility Criterion of Screw Dislocations

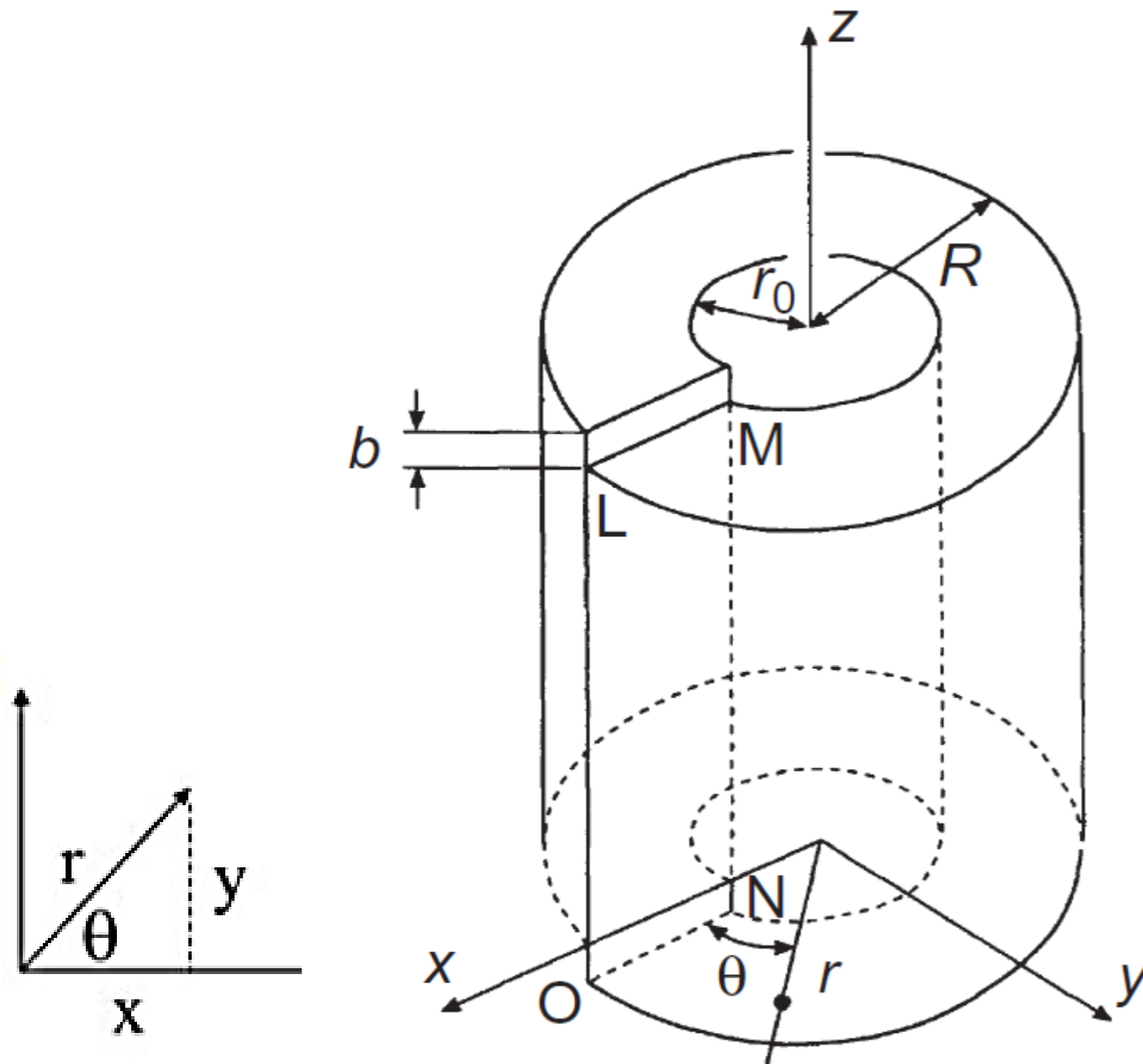
Shear Deformation along z
directions on (r,z) plane

$$u_r = u_\theta = 0 \quad u_z = \frac{b\theta}{2\pi}$$

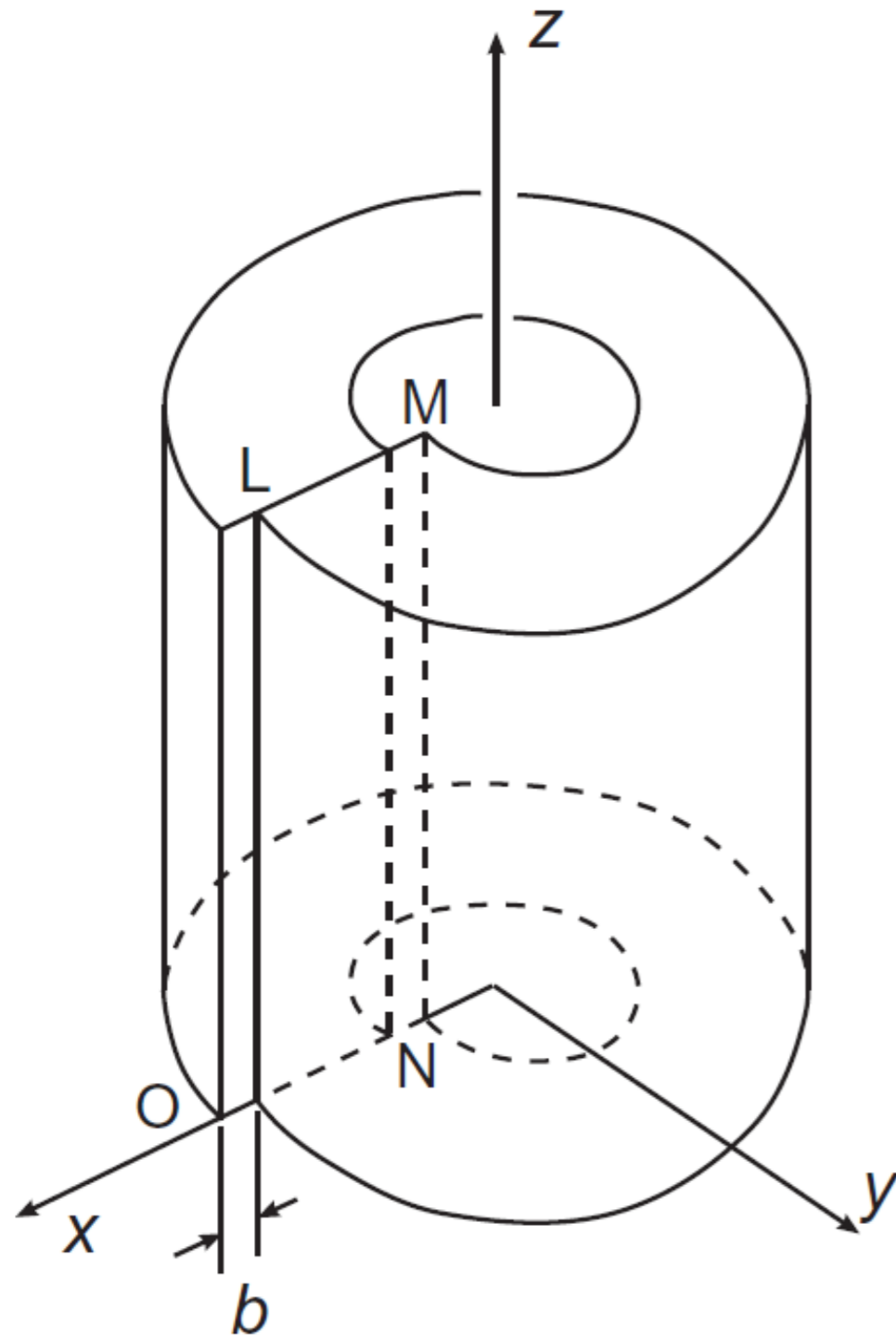
$$R(x, y) = \frac{b}{2\pi} \tan^{-1} \left(\frac{x}{y} \right)$$

The contrast extinction
condition require

$$\mathbf{g} \cdot \mathbf{R} = 0, \pm 1, \dots \rightarrow \mathbf{g} \cdot \mathbf{b} = \mathbf{0}$$



Invisibility criterion for edge dislocation (isotropic)



Plane Strain of edge dislocation

$$u_z = 0 \quad u_x = \frac{b}{2\pi} \left(\theta + \frac{\sin 2\theta}{4(1-\nu)} \right)$$

$$u_y = -\frac{b}{2\pi} \left(\frac{1-2\nu}{2(1-\nu)} \ln r + \frac{\cos 2\theta}{4(1-\nu)} \right)$$

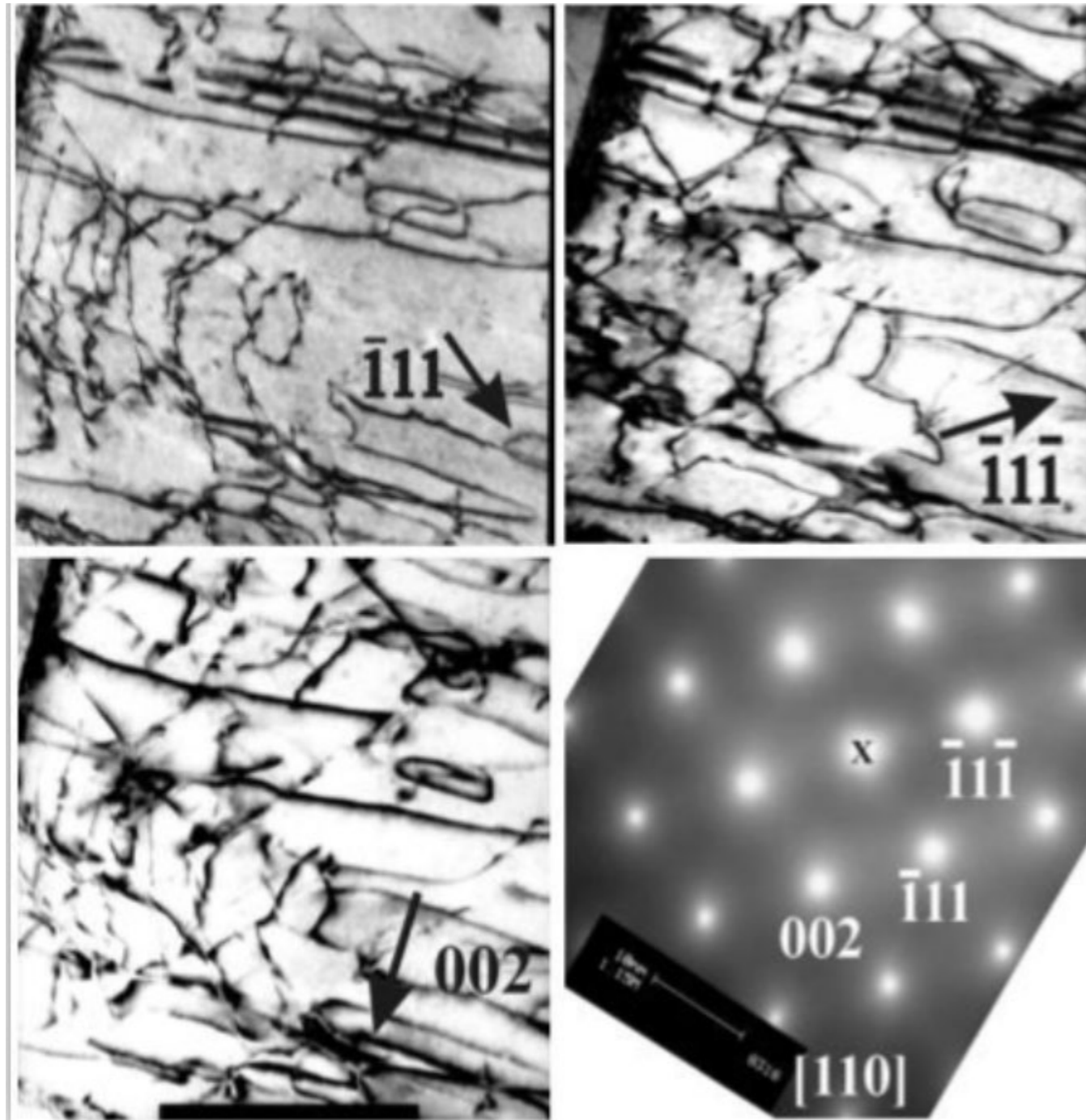
$$\mathbf{R} = \mathbf{b} \frac{\sin 2\theta}{4(1-\nu)} + \mathbf{b} \wedge \vec{\xi} \left(\frac{1-2\nu}{2(1-\nu)} \ln r + \frac{\cos 2\theta}{4(1-\nu)} \right)$$

The contrast extinction condition requires

$$\mathbf{g} \cdot \mathbf{R} = 0, \pm 1, \dots \rightarrow \mathbf{g} \cdot \mathbf{b} = 0$$

$$\mathbf{g} \cdot (\mathbf{b} \wedge \vec{\xi}) = 0 \dots \rightarrow \mathbf{g} \parallel \vec{\xi} \cdot \mathbf{b} = 0$$

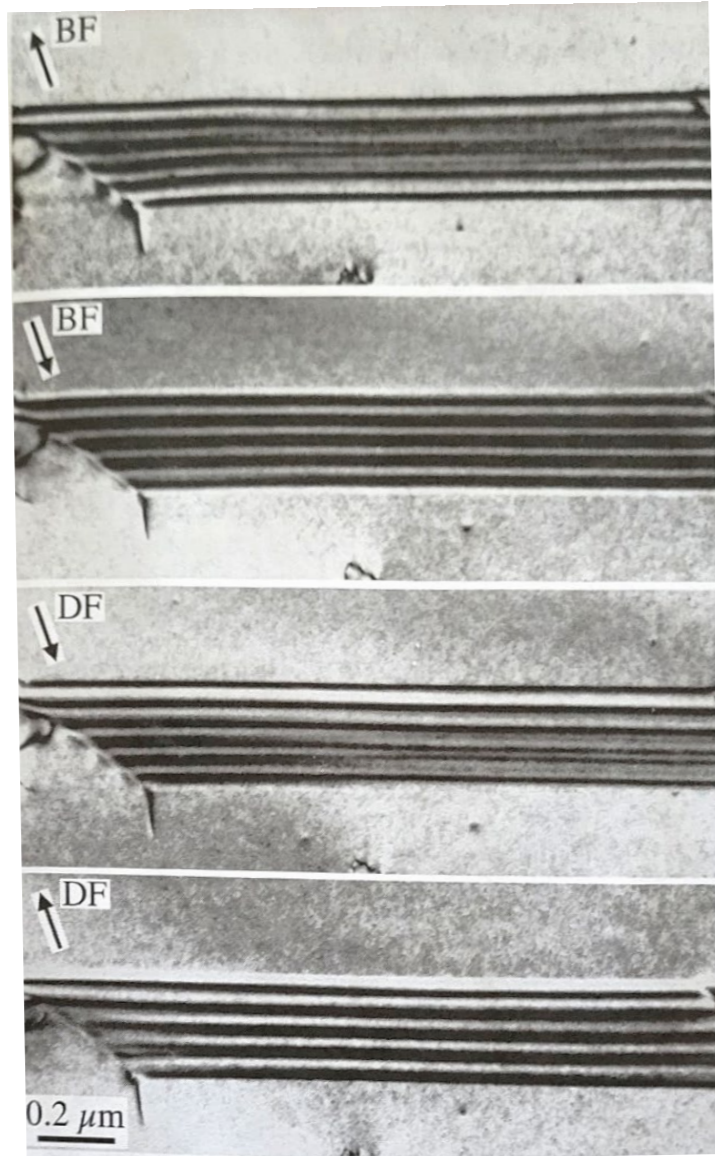
Burger's vector determination



g	b	$g \cdot b$	$g \cdot b \wedge \vec{\xi}$
$[\bar{1}11]$	$1/2[110]$	0	$\neq 0$
	$1/2[0\bar{1}1]$	0	$\neq 0$
	$1/2[101]$	0	$\neq 0$
$[\bar{1}\bar{1}1]$	$1/2[1\bar{1}0]$	-1	$\neq 0$
	$1/2[011]$	-1	$\neq 0$
	$1/2[10\bar{1}]$	-1	$\neq 0$

Possible Burger's vectors
 $[0\bar{1}1]$ and $[101]$

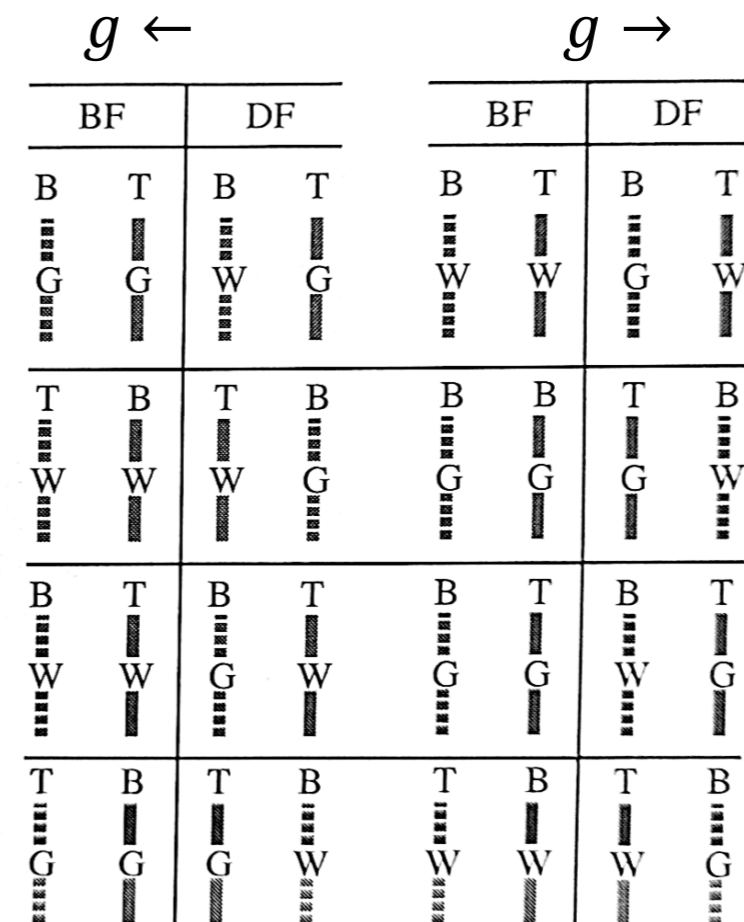
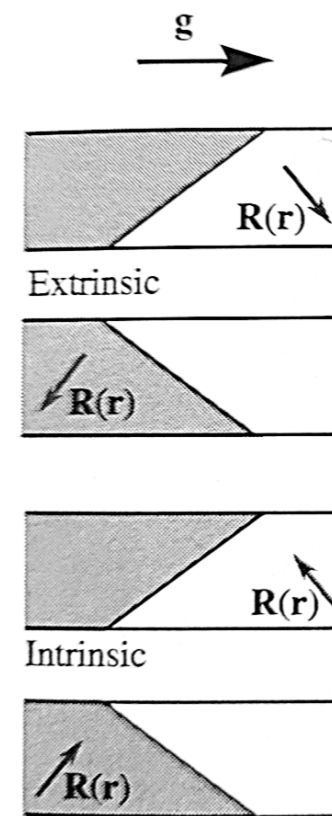
Stacking Fault Contrast



	$R(r)$	g	$2\pi g \cdot R$
SF in FCC	$1/3[111]$	(111), (220), (113)	$2\pi/3$
SF in FCC	$1/6[11\bar{2}]$	(111) (220)	0 $4\pi/3$

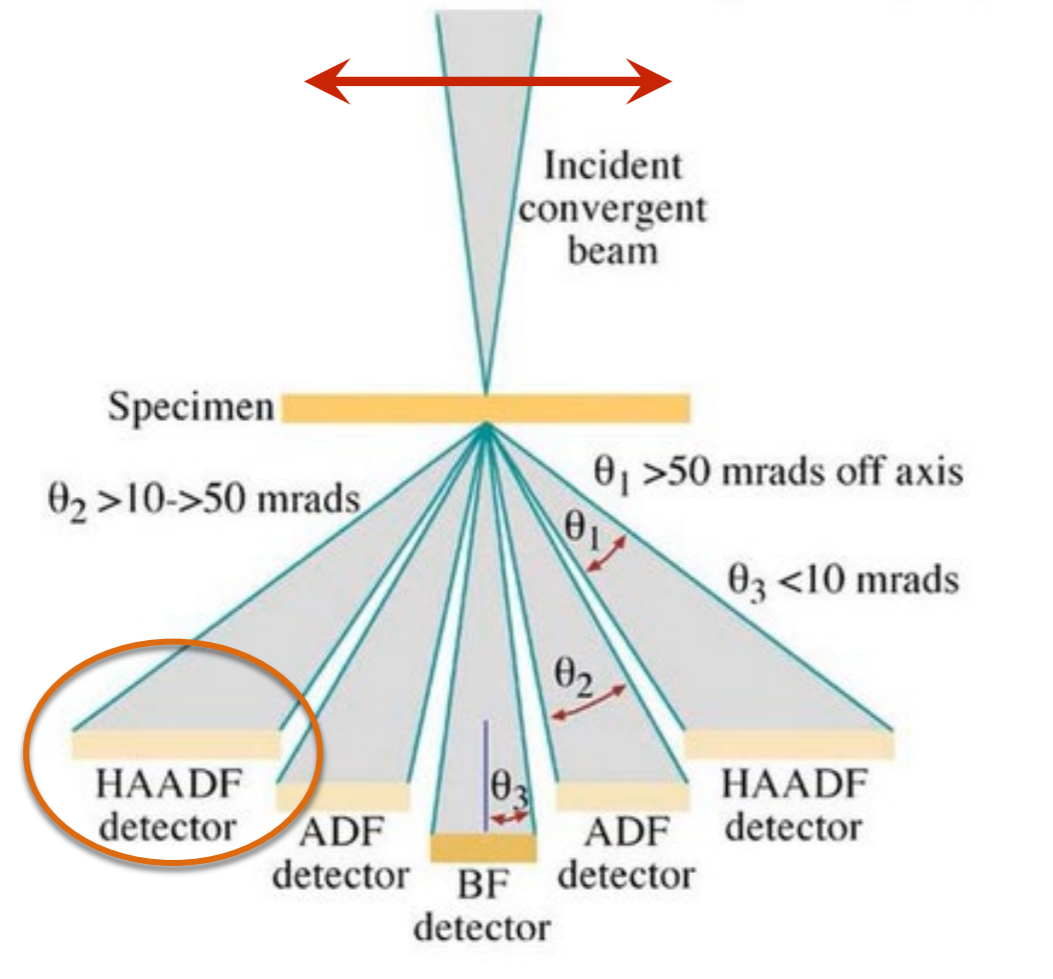
$$\frac{d\phi_g}{dz} = \frac{\pi i}{\xi_g} \phi_o(z)' + 2\pi i s_R \phi_g(z)' \text{ and}$$

$$s_R = s + g \cdot \frac{dR(r)}{dz}$$



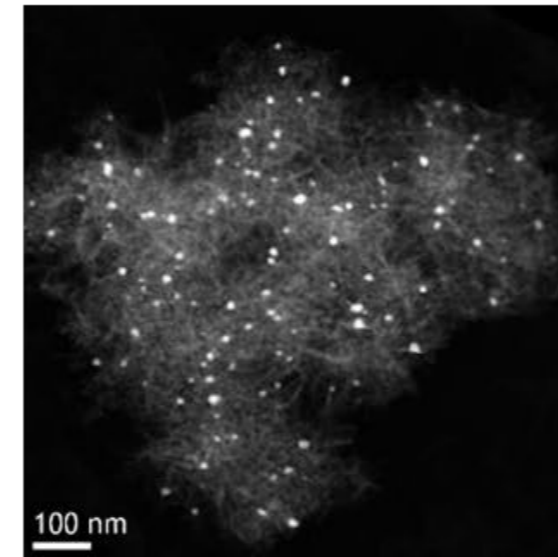
Scanning (S)TEM imaging of defects

Focused e^- probe scanned on sample; disc and annular detectors in back focal (diffraction) plane

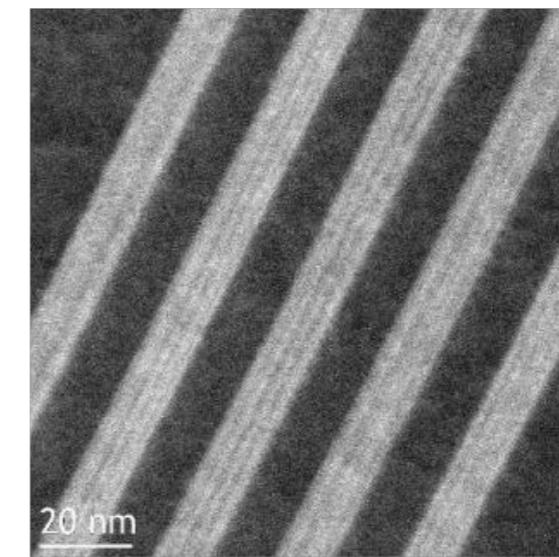


High-angle annular dark-field => compositional contrast:
intensity $\propto Z^2 t$
(thickness t , atomic number Z)

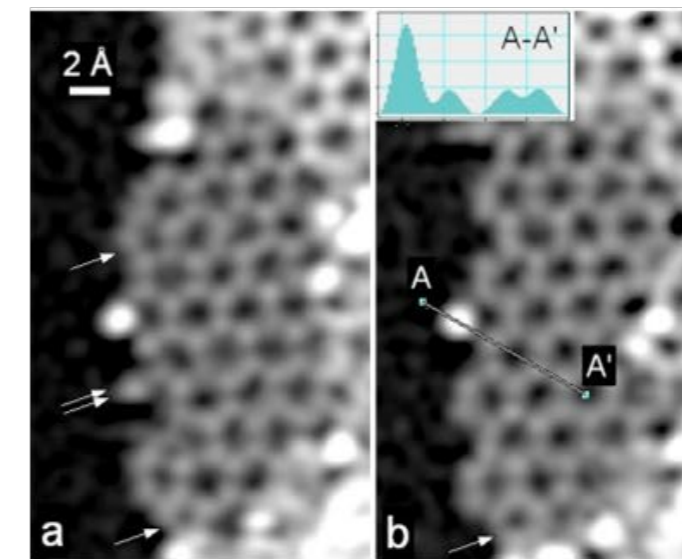
Z-contrast examples:



Pt catalyst on Al_2O_3

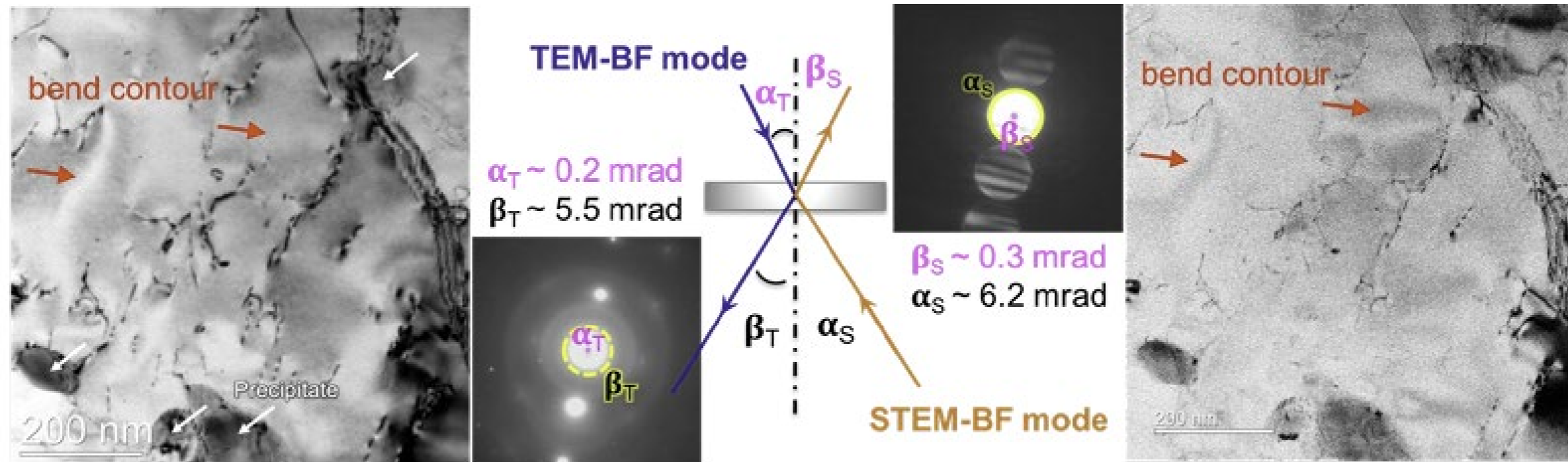


Si-Ge/Si multilayer

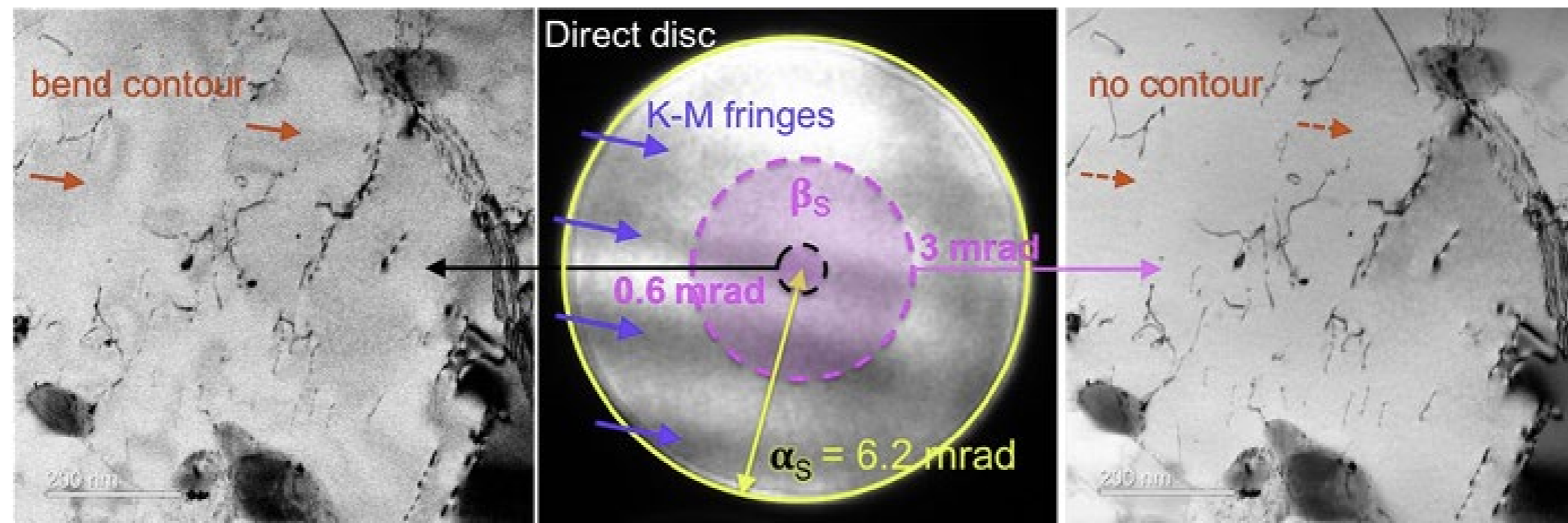


Cs-ordered - graphene with dopant atoms (Krivanek et al., Nion)

STEM imaging mode suppresses bend contours



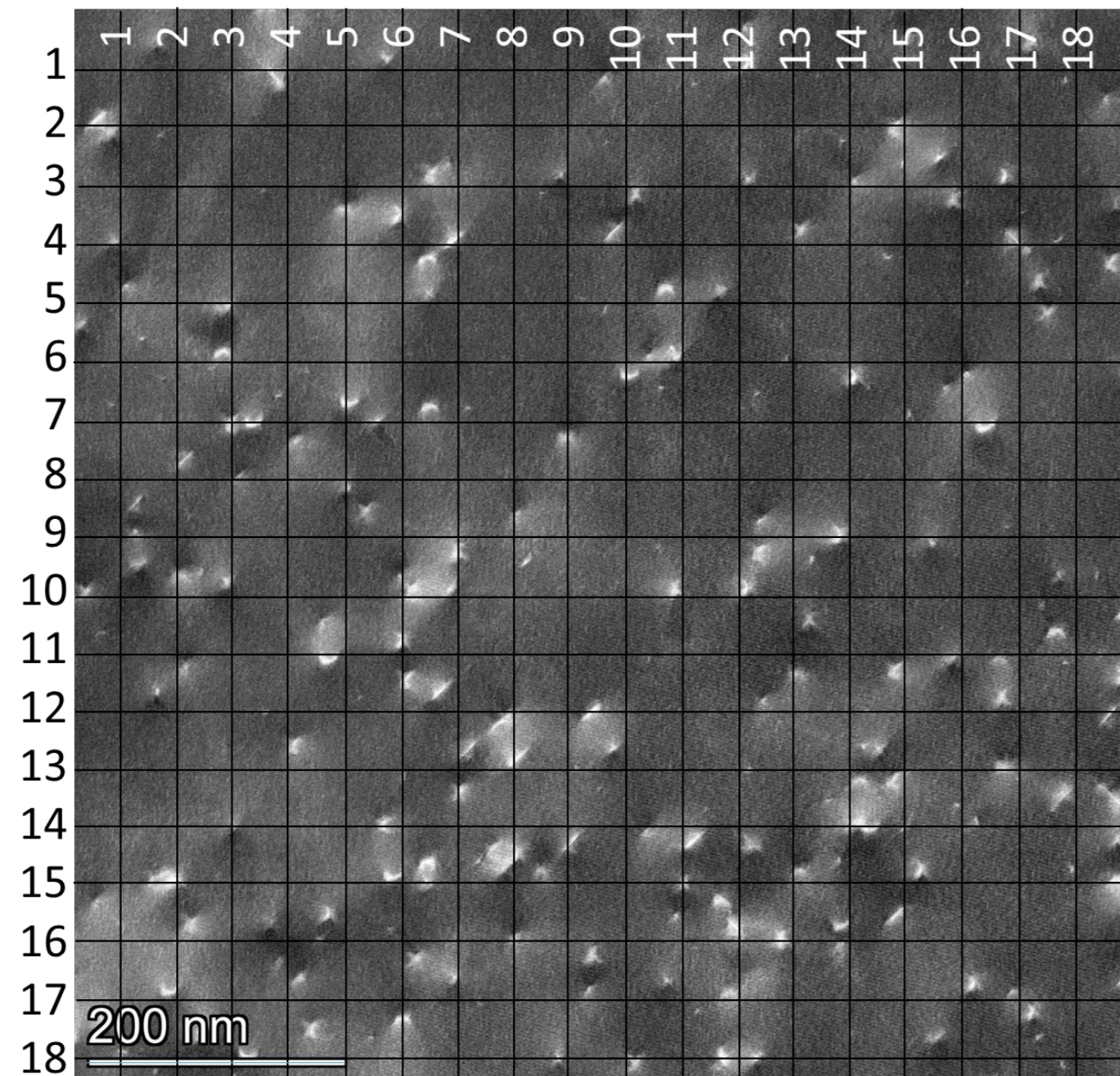
Bend Contour contrast is suppressed when $\beta_S \approx \alpha_S$



Dislocation Density Measurements

HAADF $\beta_S(24\text{mrad}) \approx \alpha_S(20\text{mrad})$

$$\Lambda \approx 5 \times 10^9 \text{ cm}^{-2}$$



Line Intercept Method

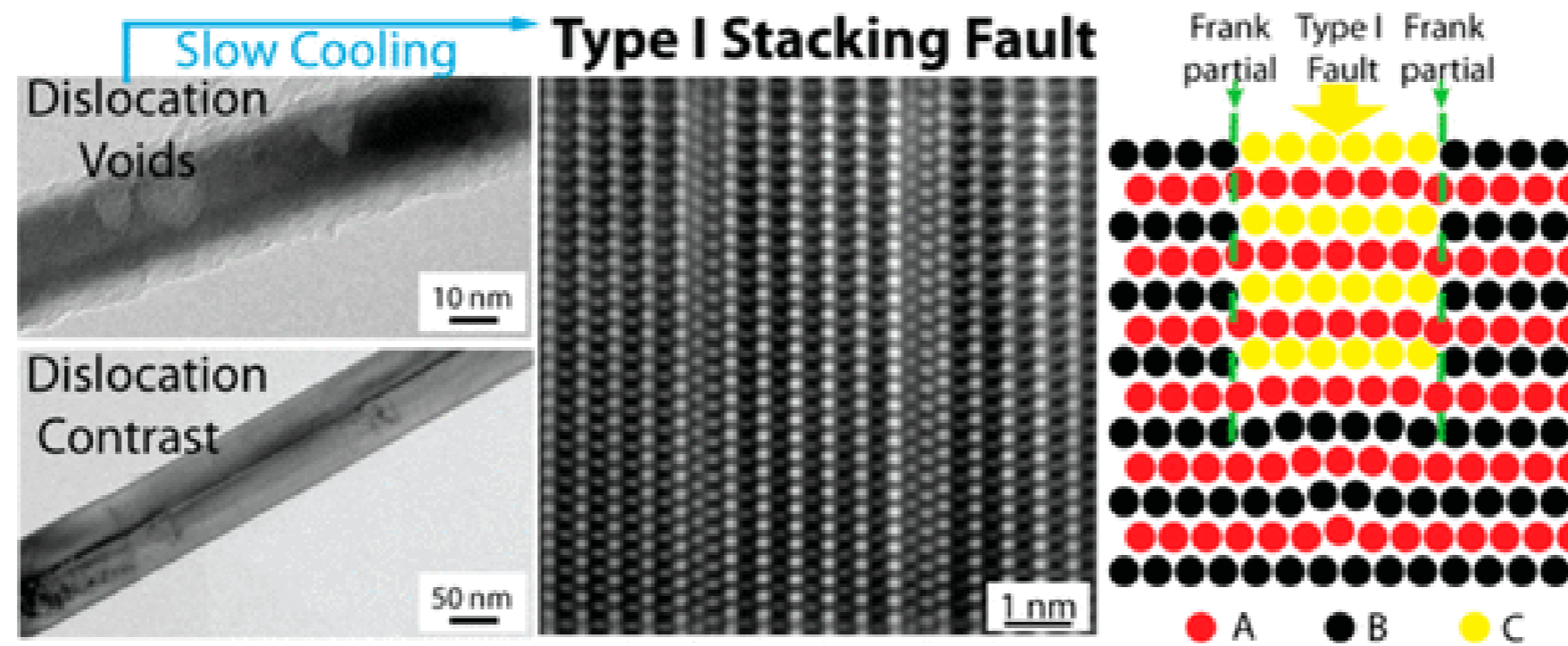
- Make a grid having a total line length L
- Count the number of intersections between a given grid and the dislocations, N
- Measure TEM sample thickness, t (EELS, CBED, X-ray reflectivity, etc.)
- The dislocation density, Λ , is given by the following equation.

$$\Lambda = 2N/tL$$

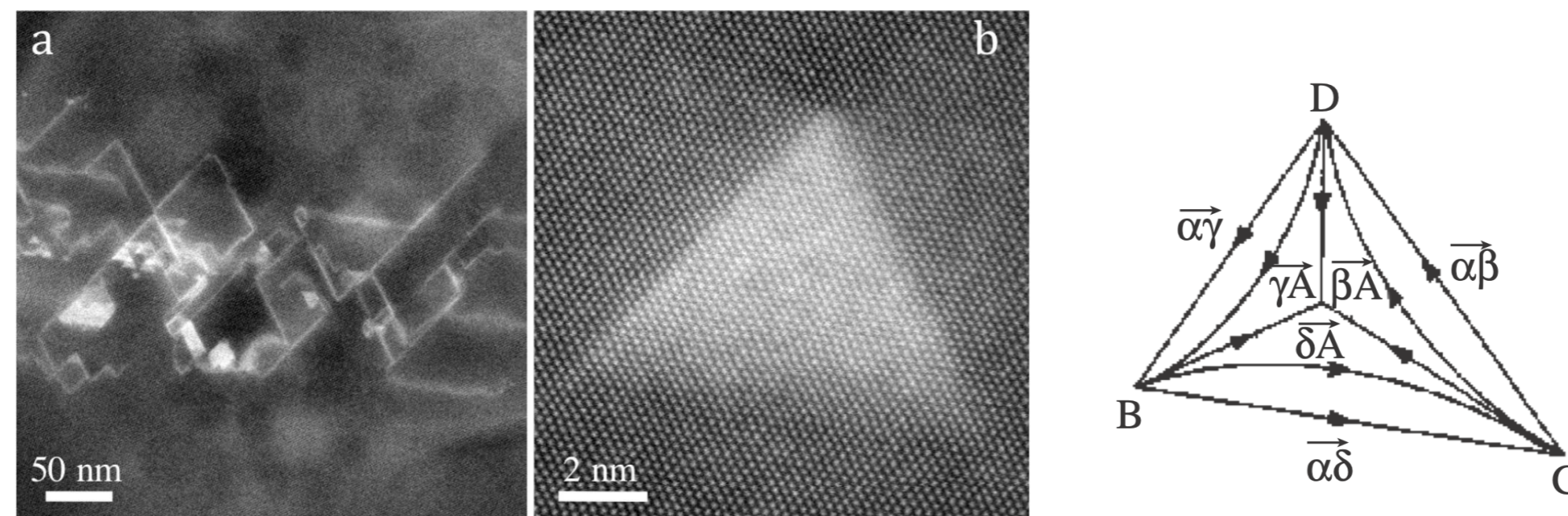
- This method is valid for dislocation density is less than 10^{14} cm^{-2} .

HR-STEM images of stacking faults

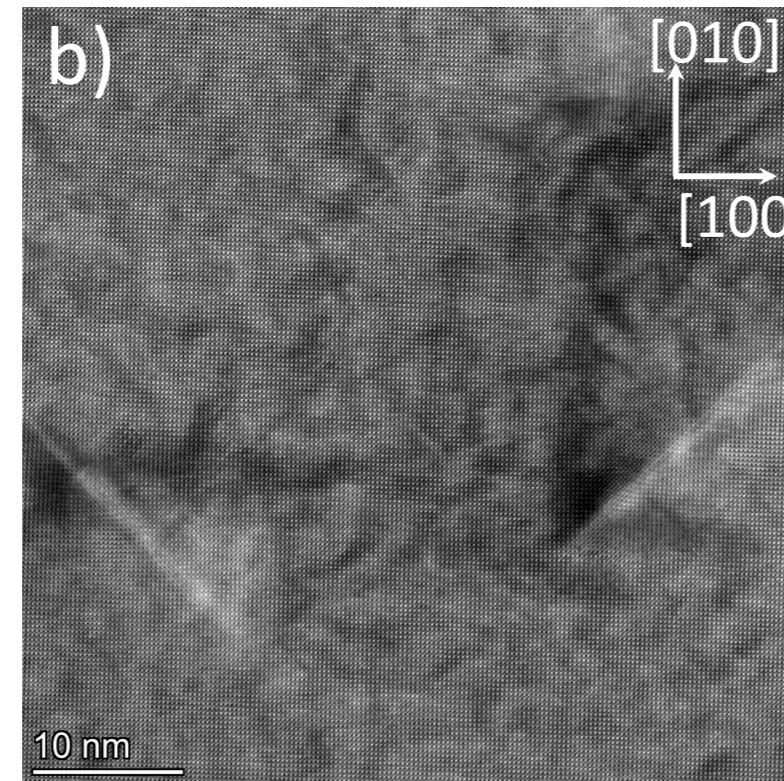
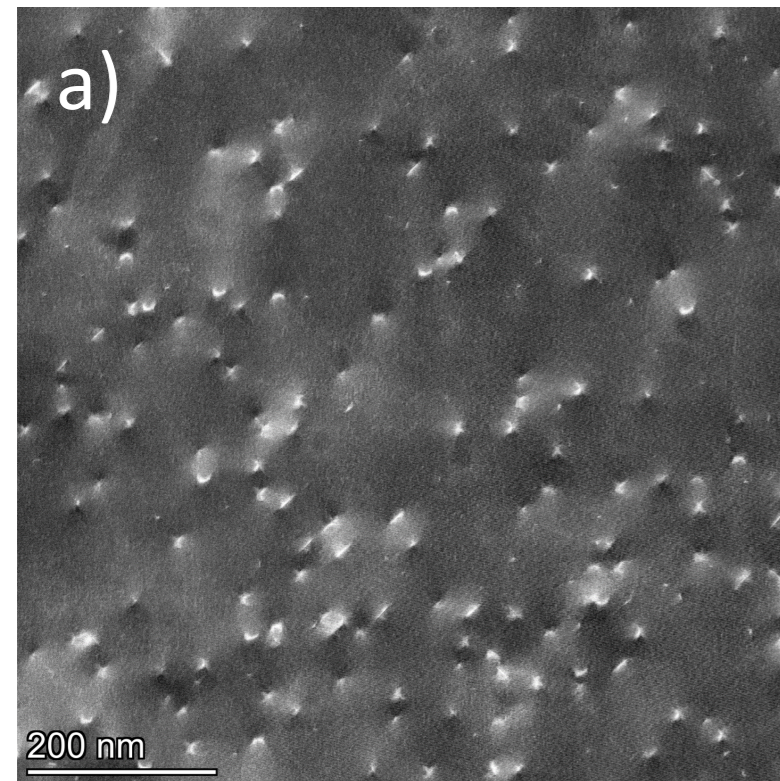
Growth faults in AlN nanowires



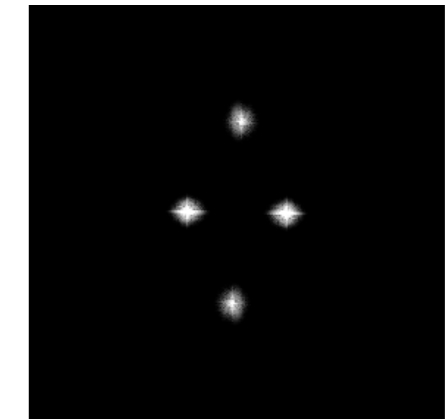
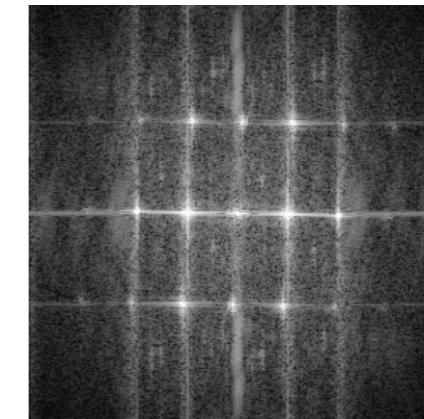
Stacking Fault Tetrahedron in FCC Superalloy



HR-STEM images of the Dislocations

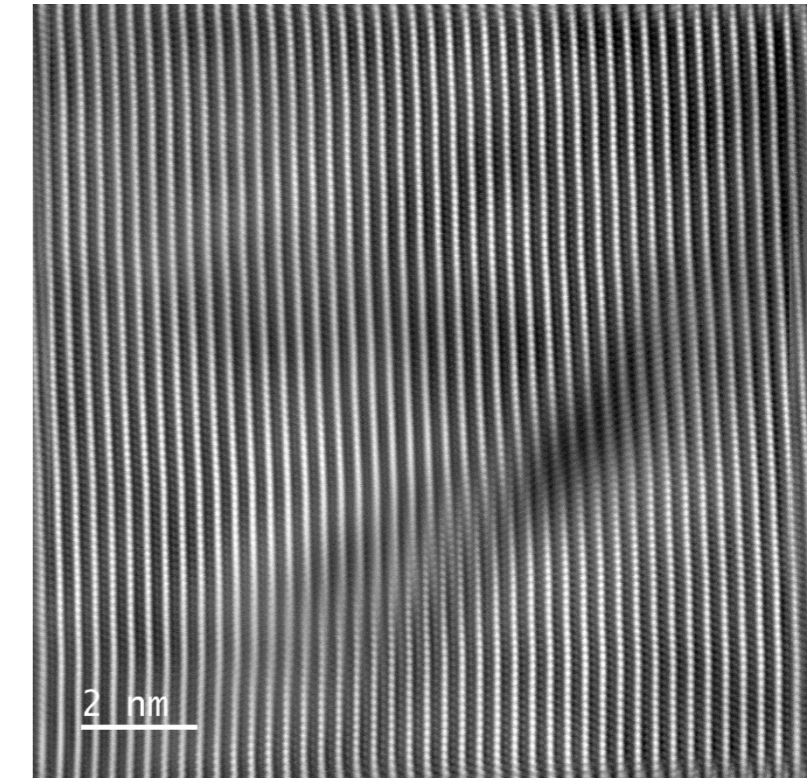
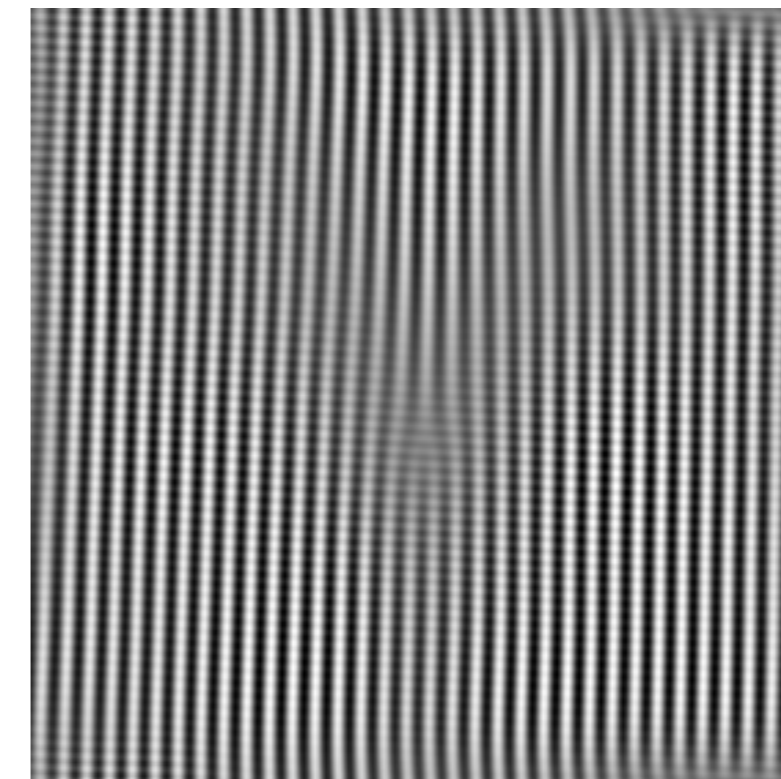
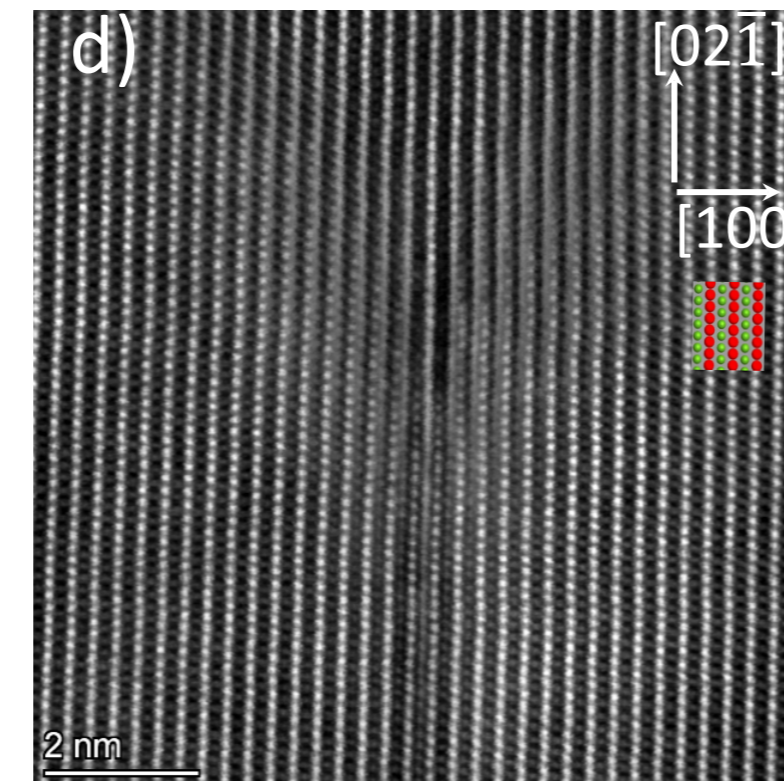
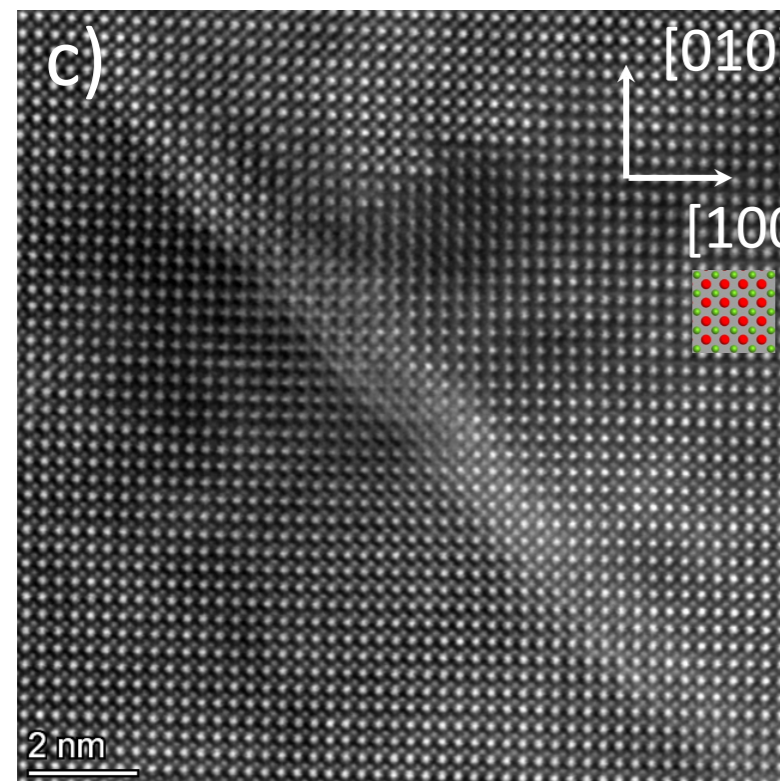


Fourier Filtering

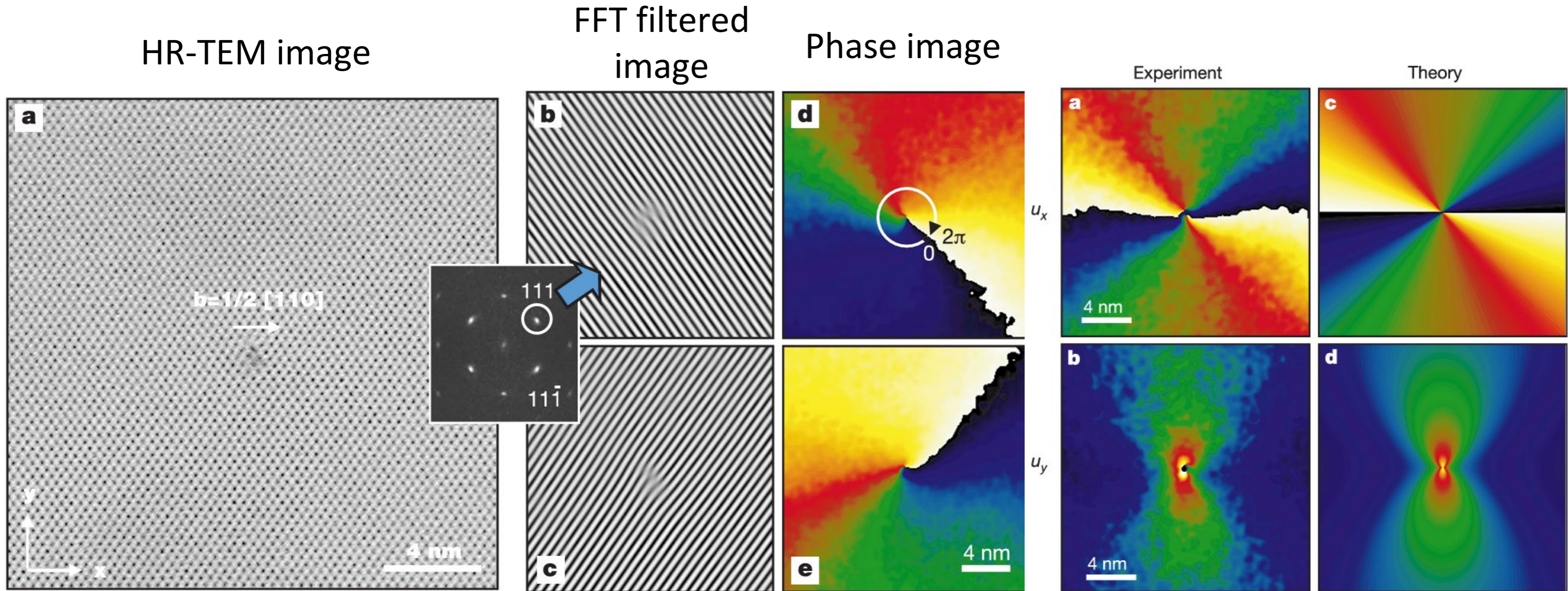


$$\vec{b} = a[100]$$

$$\vec{b} = a[111]$$



Geometric Phase Analysis of Dislocations



$$u_x = \frac{b}{2\pi} \left(\theta + \frac{\sin 2\theta}{4(1-\nu)} \right) \quad u_y = -\frac{b}{2\pi} \left(\frac{1-2\nu}{2(1-\nu)} \ln r + \frac{\cos 2\theta}{4(1-\nu)} \right)$$

HR-STEM images of the Dislocations

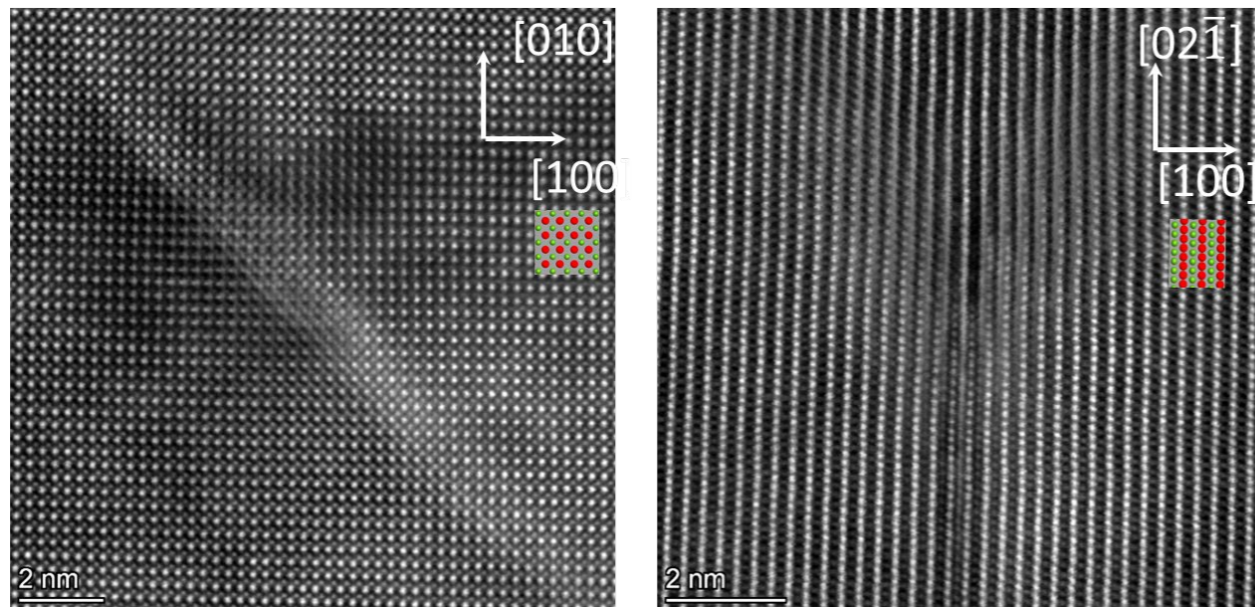
Table 1
Observed slip system in the eight B2 alloys studied.

Alloy	CuZn	FeAl	NiAl	FeTi	CoTi	NiTi	FeGa
Dominant slip directions	$\langle 111 \rangle$	$\langle 111 \rangle$	$\langle 001 \rangle$ $\langle 111 \rangle$	$\langle 001 \rangle$	$\langle 001 \rangle$	$\langle 001 \rangle$	$\langle 111 \rangle$
References	[1–5]	[6–11]	[5,12–16]	[17]	[18–23]	[9,24–27]	[28]

Table 2
Calculated and experimental lattice parameters a (Å) and elastic moduli (GPa).

Alloy	CuZn	FeAl	NiAl	FeTi	CoTi	NiTi	FeGa	PdAl
a (this work)	2.97	2.88	2.90	2.95	2.97	3.01	2.90	3.02
a (experiment) [58]	2.95	2.91	2.88	2.98	2.99	3.01	2.91 [55]	3.04
C_{11} (this work)	123.3	254.4	204.1	384.8	212.6	185.3	240.4	221.8
C_{11} (experiment)	119	194	199	310	203	162	NA	NA
C_{12} (this work)	107.3	136.1	133.2	102.8	169.5	149.7	150.2	160.9
C_{12} (experiment)	102	116	137	86	129	132	NA	NA
C_{44} (this work)	83.4	139.6	114.5	68.2	52.2	48.6	115.7	92.9
C_{44} (experiment)	74	133	116	75	68	71	~100	NA
References for experiments	[59]	[60]	[61]	[62]	[63]	[64]	[65]	

$$\vec{b} = a \langle 111 \rangle \{110\} \quad \vec{b} = a \langle 100 \rangle \{110\}$$



$$A = 2C_{44} \setminus (C_{11} - C_{12}) \quad K^{screw} = \mu b^2 / 4\pi$$

$$W \approx \frac{\mu b^2}{4\pi} \ln \frac{R}{r_0} \rightarrow \infty \quad r_0 \rightarrow 0$$

Table 3
Anisotropy factors A and energy factors K ($\text{J/m} \times 10^{-9}$) determining the elastic energy of corresponding dislocations per unit length (m).

Alloy	A	$K_{\langle 111 \rangle}^{screw}$	$K_{\langle 111 \rangle}^{edge}$	$K_{\langle 001 \rangle}^{screw}$	$K_{\langle 001 \rangle}^{edge}$	$K_{\langle 111 \rangle}^{screw} / K_{\langle 001 \rangle}^{screw}$
CuZn	10.42	0.369	1.130	0.585	0.405	0.63
FeAl	2.36	1.531	2.766	0.921	0.855	1.66
NiAl	3.23	1.028	2.152	0.766	0.671	1.34
FeTi	0.48	2.252	2.611	0.473	0.939	4.76
CoTi	2.42	0.606	1.328	0.366	0.438	1.66
NiTi	2.73	0.535	1.212	0.350	0.402	1.53
FeGa	2.56	1.218	2.388	0.774	0.750	1.57
PdAl	3.05	0.946	2.066	0.674	0.664	1.40